

Thermodynamic Assessment of the Fe-Mn-O System

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The C-Cr-Fe-Ni-O system has recently been studied with the intention to thermodynamically describe the influence of oxygen on high alloyed steels. In this study the ternary Fe-Mn-O system is assessed and part of the binary Mn-O system is reassessed. α - and β -hausmannite (Mn_3O_4) were earlier described as stoichiometric phases, but are here described using the compound energy formalism with a four sublattice model to be consistent with the preceding study of the Cr-Fe-Ni-O spinel. The liquid phase is assessed using the ionic two-sublattice model. Good agreement between calculated and experimental values is achieved.

Keywords CALPHAD, Fe-Mn-O system, thermodynamic modelling

1. Introduction

In a preceding study the C-Cr-Fe-Ni-O system^[1,2] was described. It is a basic system for describing stainless steels. In this study the Fe-Mn-O system is assessed, a first step towards a consistent C-Cr-Fe-Mn-Ni-O database. In the present work both the metallic and the oxide liquid are modelled using the ionic two-sublattice model.^[3,4] The ionic two-sublattice liquid model was developed within the framework of the compound energy formalism (CEF),^[5] which is used to describe phases using two or more sublattices and is widely used in CALPHAD assessments.^[6,7]

The Fe-O system was assessed by Sundman,^[8] and later modified by Selleby and Sundman^[9] (ionic liquid), Kowalski and Spencer^[10] (fcc and bcc) and Kjellqvist et al.^[11] (hematite). This modified description of Sundmans assessment is used in this study. The Mn-O system has been assessed by Grundy et al.,^[11] and is here accepted after slight modifications. Grundy et al. described α - and β -hausmannite (Mn_3O_4) as stoichiometric phases where each component can reside in only one sublattice, thus without the possibility to describe any degree of inversion. Those phases are now treated using a more complex model, where the degree of inversion and also the deviation from stoichiometry are described. In their model for the ionic liquid they use a Mn^{+3} species which now is replaced by a neutral $\text{MnO}_{1.5}$ species equivalent to the description of the Fe-O system. For the third binary, Fe-Mn, the assessment of Huang^[12] is accepted without modification. The ternary system, Fe-Mn-O, has been assessed by Weiland,^[13] but is reassessed in this work. Weiland used a different description of the Mn-O system and the α - and β -spinel phases were

modelled as stoichiometric phases with respect to oxygen. Pelton et al.^[14] performed an assessment on the Fe_3O_4 - Mn_3O_4 system.

Some phases undergo a magnetic transition characterized by a λ -peak in the heat capacity curve. The magnetic contribution to the Gibbs energy is given by a model proposed by Inden^[15] and adapted by Hillert and Jarl.^[16]

2. Thermodynamic Models

2.1 Liquid

Grundy et al.^[11] applied the ionic two-sublattice liquid model^[3,4] to the Mn-O system, using the formula $(\text{Mn}^{2+}, \text{Mn}^{3+})_P(\text{O}^{2-}, \text{Va}^{\ominus})_Q$. The liquid phase in the Fe-O system was first modelled with $(\text{Fe}^{2+}, \text{Fe}^{3+})_P(\text{O}^{2-}, \text{Va}^{\ominus})_Q$,^[8] but later Fe^{3+} was replaced by a neutral species, $\text{FeO}_{1.5}$.^[9] This change was imposed by an equivalent change for Al-containing system where Al^{3+} was replaced by $\text{AlO}_{1.5}$ in order to better control the unwanted reciprocal miscibility gaps that occurred in e.g. Al_2O_3 -CaO-SiO₂. However, even though a new model for liquid Al_2O_3 (without $\text{AlO}_{1.5}$) has been developed,^[17] the $\text{FeO}_{1.5}$ species has been kept. In the present work the formula $(\text{Fe}^{2+}, \text{Mn}^{2+})_P(\text{O}^{2-}, \text{Va}^{\ominus}, \text{FeO}_{1.5}, \text{MnO}_{1.5})_Q$ will be used. P and Q is the number of sites on each sublattice. P and Q vary so that electroneutrality is maintained. The same model can be used both for metallic and oxide melts. At low levels of oxygen, the model becomes equivalent to a substitutional solution model between metallic atoms. The Gibbs energy of the liquid phase is expressed by:

$$\begin{aligned}
 G_m = & y_{\text{Fe}^{2+}}y_{\text{O}^{2-}}{}^{\circ}G_{\text{Fe}^{2+};\text{O}^{2-}} + y_{\text{Mn}^{2+}}y_{\text{O}^{2-}}{}^{\circ}G_{\text{Mn}^{2+};\text{O}^{2-}} \\
 & + Qy_{\text{Va}^{\ominus}}(y_{\text{Fe}^{2+}}{}^{\circ}G_{\text{Fe}^{2+};\text{Va}^{\ominus}} + y_{\text{Mn}^{2+}}{}^{\circ}G_{\text{Mn}^{2+};\text{Va}^{\ominus}}) \\
 & + Q(y_{\text{FeO}_{1.5}}{}^{\circ}G_{\text{FeO}_{1.5}} + y_{\text{MnO}_{1.5}}{}^{\circ}G_{\text{MnO}_{1.5}}) \\
 & + \text{RTP}(y_{\text{Fe}^{2+}}\ln(y_{\text{Fe}^{2+}})) + y_{\text{Mn}^{2+}}\ln(y_{\text{Mn}^{2+}}) \\
 & + \text{RTQ}(y_{\text{O}^{2-}}\ln(y_{\text{O}^{2-}}) + y_{\text{Va}^{\ominus}}\ln(y_{\text{Va}^{\ominus}}) \\
 & + y_{\text{FeO}_{1.5}}\ln(y_{\text{FeO}_{1.5}}) + y_{\text{MnO}_{1.5}}\ln(y_{\text{MnO}_{1.5}})) + {}^{\text{E}}G_m
 \end{aligned}
 \tag{Eq 1}$$

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where y denotes the site-fraction and ${}^E G_m$ is the excess Gibbs energy which depends on the interaction between species within each sublattice. The interaction parameters used in this assessment are the following:

$$\begin{aligned}
 {}^E G_m = & y_{\text{Fe}^{2+}} y_{\text{Mn}^{2+}} y_{\text{O}^{2-}} \left({}^0 L_{\text{Fe}^{2+}, \text{Mn}^{2+}; \text{O}^{2-}} + {}^1 L_{\text{Fe}^{2+}, \text{Mn}^{2+}; \text{Va}} (y_{\text{Fe}^{2+}} - y_{\text{Mn}^{2+}}) \right) \\
 & + Q y_{\text{Va}}^2 y_{\text{Fe}^{2+}} y_{\text{Mn}^{2+}} \left({}^0 L_{\text{Fe}^{2+}, \text{Mn}^{2+}; \text{Va}} + {}^1 L_{\text{Fe}^{2+}, \text{Mn}^{2+}; \text{Va}} (y_{\text{Fe}^{2+}} - y_{\text{Mn}^{2+}}) \right) \\
 & + y_{\text{Va}} y_{\text{Fe}^{2+}} y_{\text{O}^{2-}} \left({}^0 L_{\text{Fe}^{2+}; \text{O}^{2-}, \text{Va}} + {}^1 L_{\text{Fe}^{2+}; \text{O}^{2-}, \text{Va}} (y_{\text{O}^{2-}} - y_{\text{Va}}) \right) \\
 & + y_{\text{Va}} y_{\text{Mn}^{2+}} y_{\text{O}^{2-}} \left({}^0 L_{\text{Mn}^{2+}; \text{O}^{2-}, \text{Va}} + {}^1 L_{\text{Mn}^{2+}; \text{O}^{2-}, \text{Va}} (y_{\text{O}^{2-}} - y_{\text{Va}}) \right) \\
 & + y_{\text{Fe}^{2+}} y_{\text{O}^{2-}} y_{\text{FeO}_{1.5}} \left({}^0 L_{\text{Fe}^{2+}; \text{O}^{2-}, \text{FeO}_{1.5}} + {}^1 L_{\text{Fe}^{2+}; \text{O}^{2-}, \text{FeO}_{1.5}} (y_{\text{O}^{2-}} - y_{\text{FeO}_{1.5}}) \right) \\
 & + y_{\text{Mn}^{2+}} y_{\text{O}^{2-}} y_{\text{FeO}_{1.5}} {}^0 L_{\text{Mn}^{2+}; \text{O}^{2-}, \text{FeO}_{1.5}} + y_{\text{Mn}^{2+}} y_{\text{O}^{2-}} y_{\text{MnO}_{1.5}} {}^0 L_{\text{Mn}^{2+}; \text{O}^{2-}, \text{MnO}_{1.5}} \\
 & + Q y_{\text{Va}} (y_{\text{Fe}^{2+}} y_{\text{FeO}_{1.5}} {}^0 L_{\text{Fe}^{2+}; \text{FeO}_{1.5}, \text{Va}} + y_{\text{Fe}^{2+}} y_{\text{MnO}_{1.5}} {}^0 L_{\text{Fe}^{2+}; \text{MnO}_{1.5}, \text{Va}} \\
 & + y_{\text{Mn}^{2+}} y_{\text{FeO}_{1.5}} {}^0 L_{\text{Mn}^{2+}; \text{FeO}_{1.5}, \text{Va}} + y_{\text{Mn}^{2+}} y_{\text{MnO}_{1.5}} {}^0 L_{\text{Mn}^{2+}; \text{MnO}_{1.5}, \text{Va}})
 \end{aligned} \tag{Eq 2}$$

A colon is used to separate species on different sublattices and a comma is used to separate species on the same sublattice.

2.2 Spinel: Cubic and Tetragonal

There are two types of spinel phases in the Fe-Mn system; cubic and tetragonal spinels (Strukturbericht H1₁ for cubic spinel). Hausmannite (Mn₃O₄) is a tetragonal spinel (α -Mn₃O₄) at low temperatures and transforms to a cubic spinel (β -Mn₃O₄) at higher temperatures. α -Mn₃O₄ dissolves small amounts of Fe, while β -Mn₃O₄ extend up to magnetite (Fe₃O₄). The tetragonal distortion originates from the Jahn-Teller distortion^[18] of octahedral sites occupied by Mn³⁺ ions.

Dorris and Mason^[19] found that α - and β -Mn₃O₄ have different ionic configuration. They believe that α -Mn₃O₄ has the same ionic configuration as cubic Fe₃O₄: (Mn²⁺, Mn³⁺)₁ (Mn²⁺, Mn³⁺)₂ (O²⁻)₄, while in the case of β -Mn₃O₄ Mn²⁺ resides on tetrahedral sites and Mn²⁺, Mn³⁺ and Mn⁴⁺ on octahedral sites: (Mn²⁺)₁ (Mn²⁺, Mn³⁺, Mn⁴⁺)₂ (O²⁻)₄. Other authors conclude that these charge states are Mn²⁺ and Mn³⁺ for both phases, see for example Ref 20-23. Taking other manganese containing spinels into consideration, e.g. the Mn-Ni system, the model with Mn⁴⁺ ions is preferred. β -Spinel dissolve more nickel than NiMn₂O₄, thus β -spinel in Mn-Ni can not sufficiently be described without using Mn⁴⁺ ions on octahedral sites. In this work it is assumed that α - and β -Mn₃O₄ have different ionic configurations: stoichiometric α -Mn₃O₄ is described by (Mn²⁺, Mn³⁺)₁ (Mn²⁺, Mn³⁺)₂ (O²⁻)₄ and β -Mn₃O₄ by (Mn²⁺)₁ (Mn²⁺, Mn³⁺, Mn⁴⁺)₂ (O²⁻)₄.

3. Cubic Hausmannite (β -Mn₃O₄)

The complete description of the spinel phase is rather complicated why a stoichiometric spinel is considered as a

first approach, which is modelled using the formula (Mn²⁺)₁ (Mn²⁺, Mn³⁺, Mn⁴⁺)₂ (O²⁻)₄. The first sublattice represents tetrahedral sites and the second sublattice represents octahedral sites. A normal spinel has the trivalent ions

on the octahedral sites and the divalent ions on the tetrahedral sites. If the octahedral sites are occupied by divalent and tetravalent ions the spinel is referred to as inverse. The three ${}^{\circ}G$ parameters (${}^{\circ}G_{\text{Mn}^{2+}; \text{Mn}^{2+}}^{\beta}$, ${}^{\circ}G_{\text{Mn}^{2+}; \text{Mn}^{3+}}^{\beta}$, and ${}^{\circ}G_{\text{Mn}^{2+}; \text{Mn}^{4+}}^{\beta}$) are from now on denoted ${}^{\circ}G_{22}^{\beta}$, ${}^{\circ}G_{23}^{\beta}$, and ${}^{\circ}G_{24}^{\beta}$. The Gibbs energy of stoichiometric β -Mn₃O₄ is given by

$${}^{\circ}G_m^{\beta} = y'_2 y''_2 {}^{\circ}G_{22}^{\beta} + y'_2 y''_3 {}^{\circ}G_{23}^{\beta} + y'_2 y''_4 {}^{\circ}G_{24}^{\beta} - \text{TS}_m + {}^E G_m \tag{Eq 3}$$

where the superscripts ' and '' denote tetrahedral and octahedral sites, respectively. This is a system with a neutral line between the ${}^{\circ}G_{23}^{\beta}$ corner and the middle of the ${}^{\circ}G_{22}^{\beta} - {}^{\circ}G_{24}^{\beta}$ side. All points on the neutral line between the normal and inverse spinels represent the stoichiometric composition, but with different distributions of ions on the octahedral sublattice. Only one point on the line represents the equilibrium composition at a given temperature. Only two parameters can normally be evaluated since there are two pieces of information, the Gibbs energy of the equilibrium phase and the degree of inversion. The site fractions in Eq 3 are replaced by a variable describing the disorder, ξ . $\xi = 0$ yields the normal state (Mn²⁺)₁ (Mn³⁺)₂ and $\xi = 1$ yields the inverse state (Mn²⁺)₁ (Mn²⁺_{0.5}, Mn⁴⁺_{0.5})₂. ξ is an expression of the degree of inversion and can be used to express all site fractions, $\xi = 1 - y'_3 = 2y''_2 = 2y''_4$, $y'_2 = 1$. All interaction energies in Eq 3 should be neglected since there already are more compound energies than experimental information, i.e. ${}^E G_m$ is set to zero. Rearranging Eq 3 and expressing all site fractions in terms of ξ yields:

$$G_m^{\beta} + \text{TS}_m(\xi) = {}^{\circ}G_{23}^{\beta} + J_{234}^{\beta} \xi \tag{Eq 4}$$

$$J_{234}^{\beta} = 0.5 {}^{\circ}G_{22}^{\beta} + 0.5 {}^{\circ}G_{24}^{\beta} - {}^{\circ}G_{23}^{\beta} \tag{Eq 5}$$

Gibbs energy of β - Mn_3O_4 is given by the parameter ${}^\circ G_{23}^\beta$ and J_{234}^β is used to model the degree of inversion. ${}^\circ G_{22}^\beta$ is used as a reference and can adopt any value. If Mn-O was assessed without the intention to include the description in a larger system the easiest choice would be to put ${}^\circ G_{22}^\beta = 0$. But since a reference already is chosen in Fe_3O_4 , ${}^\circ G_{22}^\beta$ will adopt a value from the Fe-Mn-O assessment that is compatible with the reference in Fe-O. This gives the following parameters for stoichiometric β - Mn_3O_4 :

$${}^\circ G_{22}^\beta \text{ reference} \quad (\text{Eq 6})$$

$${}^\circ G_{23}^\beta = 7G_{\text{Mn}_3\text{O}_4}^\beta \quad (\text{Eq 7})$$

$${}^\circ G_{24}^\beta = 14G_{\text{Mn}_3\text{O}_4}^\beta + J_{\text{Mn}_3\text{O}_4}^\beta - {}^\circ G_{22}^\beta \quad (\text{Eq 8})$$

β - Mn_3O_4 shows a small deviation from stoichiometry. Vacant sites are formed in the octahedral sublattice to maintain electroneutrality when excess Mn^{4+} is introduced to model the deviation towards oxygen in equilibrium with Mn_2O_3 . The extended spinel model is then $(\text{Mn}^{2+})_1(\text{Mn}^{2+}, \text{Mn}^{3+}, \text{Mn}^{4+}, \text{Va})_2(\text{O}^{2-})_4$. Several combinations to form neutral Mn_2O_3 with spinel structure are found in this formula. One of them is used to describe the deviation from stoichiometry towards oxygen. Gibbs energy of this Mn_2O_3 is

$${}^\circ G_{\text{m}}^\beta = \left(2{}^\circ G_{23}^\beta + 3{}^\circ G_{24}^\beta + {}^\circ G_{2\text{V}}^\beta - 2RT(6 \ln(6) - 3 \ln(3) - 2 \ln(2)) \right) / 6 \quad (\text{Eq 9})$$

where ${}^\circ G_{2\text{V}}^\beta$ is used to describe the solubility of O in the spinel. To model deviation towards manganese in equilibrium with halite, Mn^{2+} is assumed to enter interstitial sites normally filled with vacancies. The final spinel model for β - Mn_3O_4 is $(\text{Mn}^{2+})_1(\text{Mn}^{2+}, \text{Mn}^{3+}, \text{Mn}^{4+}, \text{Va})_2(\text{Mn}^{2+}, \text{Va})_2(\text{O}^{2-})_4$. A new neutral endpoint is found, a hypothetical metastable MnO with spinel structure. Gibbs energy of this endpoint is

$${}^\circ G_{\text{m}}^\beta = \left({}^\circ G_{22\text{V}}^\beta + {}^\circ G_{222}^\beta - 4RT \ln(2) \right) / 2 \quad (\text{Eq 10})$$

where ${}^\circ G_{222}^\beta$ is used to describe the solubility of Mn in the spinel. The remaining three ${}^\circ G$ parameters (${}^\circ G_{232}^\beta$, ${}^\circ G_{242}^\beta$, and ${}^\circ G_{2\text{V}2}^\beta$) are obtained from reciprocal reactions ($\Delta G_{223:2\text{V}2}$, $\Delta G_{224:2\text{V}2}$, $\Delta G_{22\text{V}:2\text{V}2}$), where all reactions are assumed to have $\Delta G = 0$.

4. Tetragonal Hausmannite (α - Mn_3O_4)

The stoichiometric tetragonal spinel is modelled using the formula $(\text{Mn}^{2+}, \text{Mn}^{3+})_1(\text{Mn}^{2+}, \text{Mn}^{3+})_2(\text{O}^{2-})_4$. The four ${}^\circ G$ parameters (${}^\circ G_{\text{Mn}^{2+}:\text{Mn}^{2+}}$, ${}^\circ G_{\text{Mn}^{2+}:\text{Mn}^{3+}}$, ${}^\circ G_{\text{Mn}^{3+}:\text{Mn}^{2+}}$ and ${}^\circ G_{\text{Mn}^{3+}:\text{Mn}^{3+}}$) are from now on denoted ${}^\circ G_{22}^\alpha$,

${}^\circ G_{23}^\alpha$, ${}^\circ G_{32}^\alpha$ and ${}^\circ G_{33}^\alpha$. Gibbs energy of stoichiometric α - Mn_3O_4 is given by

$${}^\circ G_{\text{m}}^\alpha = y'_2 y''_2 {}^\circ G_{22}^\alpha + y'_2 y'_3 {}^\circ G_{23}^\alpha + y'_3 y''_2 {}^\circ G_{32}^\alpha + y'_3 y'_3 {}^\circ G_{33}^\alpha - \text{TS}_{\text{m}} + {}^E G_{\text{m}} \quad (\text{Eq 11})$$

This is a reciprocal system, with a neutral line between the ${}^\circ G_{23}^\alpha$ corner and the middle of the ${}^\circ G_{32}^\alpha - {}^\circ G_{33}^\alpha$ side. How to choose the optimizing parameters for a 23-spinel is discussed in detail by Hillert et al.^[24] The site fractions in Eq 11 are replaced by a variable describing the disorder, ξ . $\xi = 0$ yields the normal state $(\text{Mn}^{2+})_1(\text{Mn}^{3+})_2$ and $\xi = 1$ yields the inverse state $(\text{Mn}^{3+})_1(\text{Mn}_{0.5}^{2+}, \text{Mn}_{0.5}^{3+})_2$. α - Mn_3O_4 is a normal spinel with low degree of inversion. ξ is an expression of the degree of inversion and can be used to express all site fractions, $\xi = y'_3 = 1 - y'_2 = 2y''_2 = 2(1 - y'_3)$. Rearranging Eq 11, neglecting all interaction energies and expressing all site fractions in terms of ξ yields:

$$G_{\text{m}}^\alpha + \text{TS}_{\text{m}}(\xi) = {}^\circ G_{23}^\alpha + 0.5J_{23}^\alpha \xi + 0.5\Delta G_{23:23} \xi^2 \quad (\text{Eq 12})$$

$$J_{23}^\alpha = {}^\circ G_{22}^\alpha - 3{}^\circ G_{23}^\alpha + 2{}^\circ G_{33}^\alpha \quad (\text{Eq 13})$$

$$\Delta G_{23:23} = {}^\circ G_{23}^\alpha + {}^\circ G_{32}^\alpha - {}^\circ G_{22}^\alpha - {}^\circ G_{33}^\alpha \quad (\text{Eq 14})$$

Gibbs energy of α - Mn_3O_4 is given by the parameter ${}^\circ G_{23}^\alpha$ and J_{23}^α is used to model the degree of inversion. ${}^\circ G_{33}^\alpha$ is used as a reference and will adopt a value from the Fe-Mn-O assessment that is compatible with the reference in the Fe-O assessment. The last parameter, ${}^\circ G_{32}^\alpha$, is determined by the reciprocal reaction, where $\Delta G_{23:23} = 0$ is chosen. This gives the following parameters for stoichiometric α - Mn_3O_4 :

$${}^\circ G_{22}^\alpha = 21G_{\text{Mn}_3\text{O}_4}^\alpha + 2J_{\text{Mn}_3\text{O}_4}^\alpha - 2{}^\circ G_{33}^\alpha \quad (\text{Eq 15})$$

$${}^\circ G_{23}^\alpha = 7G_{\text{Mn}_3\text{O}_4}^\alpha \quad (\text{Eq 16})$$

$${}^\circ G_{32}^\alpha = 14G_{\text{Mn}_3\text{O}_4}^\alpha + 2J_{\text{Mn}_3\text{O}_4}^\alpha - {}^\circ G_{33}^\alpha \quad (\text{Eq 17})$$

$${}^\circ G_{33}^\alpha \text{ reference} \quad (\text{Eq 18})$$

In the same way as β - Mn_3O_4 , α - Mn_3O_4 also shows a small deviation from stoichiometry. The complete model is $(\text{Mn}^{2+}, \text{Mn}^{3+})_1(\text{Mn}^{2+}, \text{Mn}^{3+}, \text{Va})_2(\text{Mn}^{2+}, \text{Va})_2(\text{O}^{2-})_4$.

Two new neutral endpoints are found, hypothetical metastable Mn_2O_3 and MnO with spinel structure. The Gibbs energy of these endpoints are

$${}^\circ G_{\text{m}}^\alpha = \left(5{}^\circ G_{33\text{V}}^\alpha + {}^\circ G_{3\text{V}\text{V}}^\alpha - 2RT(6 \ln(6) - 5 \ln(5)) \right) / 6 \quad (\text{Eq 19})$$

$${}^\circ G_{\text{m}}^\alpha = \left({}^\circ G_{22\text{V}}^\alpha + {}^\circ G_{222}^\alpha - 4RT \ln(2) \right) / 2 \quad (\text{Eq 20})$$

where ${}^\circ G_{3\text{V}\text{V}}^\alpha$ and ${}^\circ G_{222}^\alpha$ are used to describe the solubility of O and Mn respectively in α -spinel. The remaining ${}^\circ G$ parameters (${}^\circ G_{2\text{V}\text{V}}^\alpha$, ${}^\circ G_{232}^\alpha$, ${}^\circ G_{2\text{V}2}^\alpha$, ${}^\circ G_{322}^\alpha$, ${}^\circ G_{332}^\alpha$, ${}^\circ G_{3\text{V}2}^\alpha$) are obtained from reciprocal reactions, where all reactions are assumed to have $\Delta G = 0$.

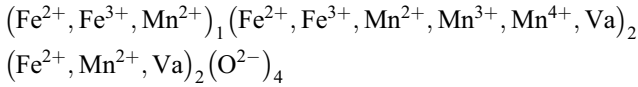
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The high temperature β - Mn_3O_4 is modelled relative to α - Mn_3O_4 by:

$${}^\circ G_{23V}^\alpha = {}^\circ G_{23V}^\beta + A + BT \quad (\text{Eq 21})$$

5. Cubic Fe-Mn Spinel

The complete cubic Fe-Mn spinel, which besides magnetite and hausmannite consists of jacobite (MnFe_2O_4), is thus modelled as:



The subsystem used to model stoichiometric jacobite is $(\text{Fe}^{3+}, \text{Mn}^{2+})_1 (\text{Fe}^{3+}, \text{Mn}^{2+})_2 (\text{O}^{2-})_4$. This reciprocal system will generate equivalent expressions as in Eq 12-14. As in the model for stoichiometric α - Mn_3O_4 , two parameters can be obtained from experiments: Gibbs energy of MnFe_2O_4 and the degree of inversion. ${}^\circ G_{\text{Mn}^{2+};\text{Fe}^{3+}}^\beta$ is used to model the Gibbs energy of jacobite ($G_{\text{MnFe}_2\text{O}_4}^\beta$), ${}^\circ G_{\text{Fe}^{3+};\text{Mn}^{2+}}^\beta$ the degree of inversion ($J_{\text{MnFe}_2\text{O}_4}^\beta$) and ${}^\circ G_{\text{Fe}^{3+};\text{Fe}^{3+}}^\beta$ is already fixed from the Fe-O assessment. The reciprocal reaction, $\Delta G_{\text{Mn}^{2+};\text{Fe}^{3+};\text{Mn}^{2+};\text{Fe}^{3+}} = 0$ will give us the ${}^\circ G_{\text{Mn}^{2+};\text{Mn}^{2+}}^\beta$ parameter which is used in the model for Mn_3O_4 . This gives the following parameters for stoichiometric MnFe_2O_4 :

$${}^\circ G_{\text{Mn}^{2+};\text{Mn}^{2+}}^\beta = 21G_{\text{MnFe}_2\text{O}_4}^\beta + 2J_{\text{MnFe}_2\text{O}_4}^\beta - 14G_{\text{Fe}_3\text{O}_4}^\beta + 2B_{\text{Fe}_3\text{O}_4}^\beta \quad (\text{Eq 22})$$

$${}^\circ G_{\text{Mn}^{2+};\text{Fe}^{3+}}^\beta = 7G_{\text{MnFe}_2\text{O}_4}^\beta \quad (\text{Eq 23})$$

$${}^\circ G_{\text{Fe}^{3+};\text{Mn}^{2+}}^\beta = 7G_{\text{Fe}_3\text{O}_4}^\beta - B_{\text{Fe}_3\text{O}_4}^\beta - 7G_{\text{MnFe}_2\text{O}_4}^\beta + {}^\circ G_{\text{Mn}^{2+};\text{Mn}^{2+}}^\beta \quad (\text{Eq 24})$$

$${}^\circ G_{\text{Fe}^{3+};\text{Fe}^{3+}}^\beta = 7G_{\text{Fe}_3\text{O}_4}^\beta - B_{\text{Fe}_3\text{O}_4}^\beta \quad (\text{Eq 25})$$

It may seem strange that the ${}^\circ G_{\text{Mn}^{2+};\text{Mn}^{2+}}^\beta$ compound involve parameters evaluated in the assessment of both Fe_3O_4 and MnFe_2O_4 although it does not contain any Fe. This arises because there could only be one ${}^\circ G$ parameter acting as reference in a phase and the reference in the spinel phase is agreed to be ${}^\circ G_{\text{Fe}^{3+};\text{Fe}^{3+}}^\beta = {}^\circ G_{\text{Fe}^{3+};\text{Fe}^{2+}}^\beta$. It would be possible to choose another reference, i.e. ${}^\circ G_{\text{Mn}^{2+};\text{Mn}^{2+}}^\beta = 0$, and adjust the Fe_3O_4 and the MnFe_2O_4 values accordingly. This would give different values on all ${}^\circ G$ parameters that have a net charge, but the description would be identical.

There are still six parameters in the Fe-Mn system needed to be fixed in a proper way (${}^\circ G_{\text{Fe}^{2+};\text{Mn}^{2+}}^\beta$, ${}^\circ G_{\text{Fe}^{2+};\text{Mn}^{3+}}^\beta$, ${}^\circ G_{\text{Fe}^{2+};\text{Mn}^{4+}}^\beta$, ${}^\circ G_{\text{Fe}^{3+};\text{Mn}^{3+}}^\beta$, ${}^\circ G_{\text{Fe}^{3+};\text{Mn}^{4+}}^\beta$ and

${}^\circ G_{\text{Mn}^{2+};\text{Fe}^{2+}}^\beta$). Some of these parameters could be obtained by setting reciprocal reactions equals zero, while others need to be evaluated using some other expressions. Another subsystem in stoichiometric Fe-Mn spinel is $(\text{Fe}^{2+}, \text{Mn}^{2+})_1 (\text{Fe}^{2+}, \text{Mn}^{3+}, \text{Mn}^{4+})_2 (\text{O}^{2-})_4$, which can be used to model one more possible neutral spinel, FeMn_2O_4 . Gibbs energy of this subsystem is given by

$$G_{\text{m}}^\beta + \text{TS}_{\text{m}}(\xi) = {}^\circ G_{\text{Fe}^{2+};\text{Mn}^{3+}}^\beta + J_{\text{FeMn}_2\text{O}_4}^\beta \xi + D_{\text{FeMn}_2\text{O}_4}^\beta \xi^2 \quad (\text{Eq 26})$$

$$J_{\text{FeMn}_2\text{O}_4}^\beta = 0.5{}^\circ G_{\text{Fe}^{2+};\text{Fe}^{2+}}^\beta + 0.5{}^\circ G_{\text{Fe}^{2+};\text{Mn}^{4+}}^\beta - 2{}^\circ G_{\text{Fe}^{2+};\text{Mn}^{3+}}^\beta + G_{\text{Mn}^{2+};\text{Mn}^{3+}}^\beta \quad (\text{Eq 27})$$

$$D_{\text{FeMn}_2\text{O}_4}^\beta = -0.5{}^\circ G_{\text{Fe}^{2+};\text{Fe}^{2+}}^\beta - 0.5{}^\circ G_{\text{Fe}^{2+};\text{Mn}^{4+}}^\beta + {}^\circ G_{\text{Fe}^{2+};\text{Mn}^{3+}}^\beta + 0.5{}^\circ G_{\text{Mn}^{2+};\text{Fe}^{2+}}^\beta + 0.5{}^\circ G_{\text{Mn}^{2+};\text{Mn}^{4+}}^\beta - {}^\circ G_{\text{Mn}^{2+};\text{Mn}^{3+}}^\beta \quad (\text{Eq 28})$$

where ξ is the degree of inversion. This is a system with a neutral line between the ${}^\circ G_{\text{Fe}^{2+};\text{Mn}^{3+}}^\beta$ corner and the ${}^\circ G_{\text{Mn}^{2+};\text{Fe}^{2+}}^\beta - {}^\circ G_{\text{Mn}^{2+};\text{Mn}^{4+}}^\beta$ side. If $D_{\text{FeMn}_2\text{O}_4}^\beta$ is assumed to be equal to zero, Eq 27 will reduce to

$$J_{\text{FeMn}_2\text{O}_4}^\beta = 0.5{}^\circ G_{\text{Mn}^{2+};\text{Fe}^{2+}}^\beta + 0.5{}^\circ G_{\text{Mn}^{2+};\text{Mn}^{4+}}^\beta - {}^\circ G_{\text{Fe}^{2+};\text{Mn}^{3+}}^\beta \quad (\text{Eq 29})$$

which is rather obvious the parameter describing the degree of inversion of FeMn_2O_4 . The Gibbs energy of FeMn_2O_4 is given by the parameter ${}^\circ G_{\text{Fe}^{2+};\text{Mn}^{3+}}^\beta$ and the third parameter, ${}^\circ G_{\text{Fe}^{2+};\text{Mn}^{4+}}^\beta$, is given by Eq 28.

The remaining three ${}^\circ G$ parameters in the stoichiometric system (${}^\circ G_{\text{Fe}^{2+};\text{Mn}^{2+}}^\beta$, ${}^\circ G_{\text{Fe}^{3+};\text{Mn}^{3+}}^\beta$ and ${}^\circ G_{\text{Fe}^{3+};\text{Mn}^{4+}}^\beta$) are related to the previously mentioned parameters by reciprocal reactions ($\Delta G_{\text{Fe}^{2+};\text{Mn}^{2+};\text{Fe}^{3+};\text{Mn}^{2+}} = \Delta G_{\text{Fe}^{3+};\text{Mn}^{2+};\text{Fe}^{3+};\text{Mn}^{3+}} = \Delta G_{\text{Fe}^{3+};\text{Mn}^{2+};\text{Mn}^{2+};\text{Mn}^{4+}} = 0$). For the nonstoichiometric system, all 26 parameters are evaluated using $\Delta G = 0$.

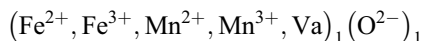
6. Tetragonal Fe-Mn Spinel

Fe has a low solubility in the tetragonal α -spinel, but to be able to correctly model the tetragonal phase, it is in this assessment described all the way to the metastable α - Fe_3O_4 . It makes very little difference what values are chosen for the majority of those parameters. We choose, rather arbitrarily, the same functions for many parameters in the tetragonal spinel as we did in the cubic spinel.

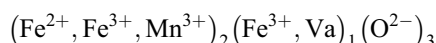
6.1 Wustite, Manganosite, Hematite, β -Bixbyite and Pyrolusite

The wustite (Fe_{1-x}O) and manganosite (Mn_{1-x}O) phases are isomorphous both having the NaCl-type structure

(Strukturbericht B1), with generic name halite. The halite phase is described using a model within the CEF with two sublattices; one for metal ions and one for oxygen. Both Fe_{1-x}O and Mn_{1-x}O have a considerable solid solubility, due to the oxidation of Fe^{2+} to Fe^{3+} and Mn^{2+} to Mn^{3+} respectively and the formation of cation vacancies. The phase is thus represented as:



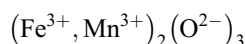
Hematite (Fe_2O_3) with the generic name corundum (Strukturbericht D5₁) is described with a small deviation from stoichiometry with a model within the CEF using three sublattices. The solubility of Mn in hematite is modelled by adding Mn^{3+} ions on the first sublattice. The phase is thus represented as:



The end member $\text{Mn}^{3+}:\text{Va}:\text{O}^{2-}$ is used to model the solubility of Mn in hematite. $\text{Mn}^{3+}:\text{Fe}^{3+}:\text{O}^{2-}$ is derived using the reciprocal reaction:

$${}^{\circ}G_{\text{Mn}^{3+}:\text{Fe}^{3+}} - {}^{\circ}G_{\text{Mn}^{3+}:\text{Va}} = {}^{\circ}G_{\text{Fe}^{3+}:\text{Fe}^{3+}} - {}^{\circ}G_{\text{Fe}^{3+}:\text{Va}}$$

α -Bixbyite ($\alpha\text{-Mn}_2\text{O}_3$) transforms to $\beta\text{-Mn}_2\text{O}_3$ (Strukturbericht D5₃) at around 300 K. The α -modification was not considered due to the low transformation temperature. The solubility of Fe in β -bixbyite is modelled by adding Fe^{3+} ions on the cation sublattice. The phase is thus represented as:



Pyrolusite (MnO_2) with the generic name rutile (Strukturbericht C4) is described as a stoichiometric phase. There are no reports on solubility of Fe in pyrolusite.

The description of Fe_{1-x}O is taken from Sundman^[8] and the description of Fe_2O_3 is from Kjellqvist et al.^[1] The descriptions for Mn_{1-x}O , $\beta\text{-Mn}_2\text{O}_3$ and MnO_2 are all from Grundy et al.^[11]

7. Experimental Data

7.1 Mn_3O_4

With increasing temperature, Mn_3O_4 transforms from tetragonal $\alpha\text{-Mn}_3\text{O}_4$ to cubic $\beta\text{-Mn}_3\text{O}_4$. The measured temperatures at which this transformation takes place varies between 1403 and 1473 K in air at 1 atmosphere total pressure, with a larger group between 1443 and 1450 K.^[20,25-34] The transformation enthalpy has been measured by three authors ranging from 18 to 22.82 kJ/mole.^[26-28] The nonstoichiometry of hausmannite has been investigated by a number of authors, some of them find it to be stoichiometric Mn_3O_4 ,^[35-39] while others find different degree of nonstoichiometry.^[20,30,31,40-46] $\beta\text{-Mn}_3\text{O}_4$ melts according to $\beta\text{-Mn}_3\text{O}_4 \rightarrow \text{liquid} + \text{gas}$. The measured temperatures ranging from 1835 to 1863 K.^[32,33,36,42,47] The eutectic between liquid $\beta\text{-Mn}_3\text{O}_4$ and halite^[33,35,36,42]

Table 1 Thermodynamic data of Mn_3O_4

	Reference
$\Delta_f^{\circ}H_{298}$, kJ/mol	
1373.27	Le Chatelier and Daubrée ^[53]
1377.46	Ruff and Gersten ^[54]
1444.45	Roth ^[55]
1408.86	Siemonsen ^[56]
1408.44	Ulich and Siemonsen ^[57]
1388.55	Shomate ^[38]
1387.09	Mah, ^[58] Zordan and Hepler ^[59]
1387.51	Robie and Waldbaum ^[60]
1388.78	Pankratz ^[25]
1386.1	Knacke et al. ^[61]
1387.4	Kubaschewski et al. ^[62]
1382.74	Grundy et al. ^[11]
1385.40	This work
${}^{\circ}S_{298}$, J/mole, K	
155.75	Pankratz ^[25]
166.6	O'Neill and Pownceby ^[63]
149.59	Millar ^[37]
164.1	Robie and Hemingway ^[64]
167.1	Chhor et al. ^[65]
154.8	Kubaschewski et al. ^[62]
154.07	Zordan and Hepler ^[59]
168.34	Grundy et al. ^[11]
165.71	This work
$\Delta H^{\alpha \rightarrow \beta}$, kJ/mol	
18	Southard and Moore ^[28]
20.9	Irani et al. ^[27]
22.82	Ramano Rao and Tare ^[26]
18.13	Pankratz ^[25]
20.8	Grundy et al. ^[11]
21.01	This work

and the reaction $\text{Mn}_2\text{O}_3 \rightarrow \beta\text{-Mn}_3\text{O}_4 + \text{gas}$ ^[25,34,36,39,48-52] have also been measured numerous times.

There are many determinations on the enthalpy of formation, $\Delta_f^{\circ}H_{298}$,^[25,38,53-62] the entropy at 298.15 K, ${}^{\circ}S_{298}$,^[25,37,59,62-65] and heat capacity, c_p ,^[37,64,65] see Table 1. The heat content of $\alpha\text{-Mn}_3\text{O}_4$ has been measured by Southard and Moore^[28] and Fritsch and Navrotsky.^[66] The magnetic transition temperature was measured by two authors^[64,65] with excellent agreement between their values, 43.15 and 43.12 K respectively.

The non-configurational free energy change on converting a normal to an inverse α -spinel ($\Delta G_D = G_i - G_n + TS_m = 0.5J_{23}^{\alpha}$) has been calculated from crystal field theory by several authors.^[21,22,67] Dorris and Mason^[19] measured the ionic configuration for $\beta\text{-Mn}_3\text{O}_4$.

7.2 Fe-Mn-O

The nonstoichiometry of $(\text{Fe}_{1-x}\text{Mn}_x)_{1-\delta}\text{O}$ has been investigated at different temperatures and compositions.^[68-72] There are a number of investigations on the two-phase region between halite and fcc^[52,68,69,72-77] and halite and spinel.^[52,68,69,72,74-80] Ref 52, 69, 73, 77, 81-83 measured the activity of FeO at the two-phase equilibrium fcc/halite.

The phase relations in the system $\text{Fe}_2\text{O}_3\text{-Mn}_2\text{O}_3$ have been examined by several authors.^[75,84-88] Bixbyite has large solubility of iron, approximately 70% at the peritectoid reaction between bixbyite, corundum and β -spinel in air, while the solubility of Mn in corundum at the same reaction is approximately 13%.

The two-phase region between corundum and spinel at 1273 K has been investigated by Ref 69, 75, 76.

Fe_3O_4 and $\beta\text{-Mn}_3\text{O}_4$ forms a continuous solid solution down to 1443 K at the manganese side, where $\beta\text{-Mn}_3\text{O}_4$ transforms to $\alpha\text{-Mn}_3\text{O}_4$. While $\beta\text{-Mn}_3\text{O}_4$ is isomorph with Fe_3O_4 , $\alpha\text{-Mn}_3\text{O}_4$ has a limited solubility of iron. The miscibility limits of the $\alpha\text{-Mn}_3\text{O}_4/\beta\text{-Mn}_3\text{O}_4$ transformation has been determined by Ref 32, 79, 86, 89-92. Jacobsite (MnFe_2O_4) is a normal spinel at low temperatures, with an increasing degree of inversion at higher temperatures. The cation distribution of jacobite has been studied by several authors.^[93-99] The oxygen nonstoichiometry of β -spinel has been measured by Bulgakov and Rozanov^[74] and Terayama et al.^[100]

The enthalpy of formation, $\Delta_f^\circ H_{298}$, and the entropy at 298.15 K, $^\circ S_{298}$, for MnFe_2O_4 are tabulated by Kubaschewski et al.^[62] Heat content, $H-H_{298}$, and heat capacity, c_p , for temperatures ranging from 298 to 1000 K have been measured by Reznitskii.^[101] Naito et al.^[102] measured c_p for the spinels MnFe_2O_4 , $\text{Mn}_{1.5}\text{Fe}_{1.5}\text{O}_4$ and Mn_2FeO_4 between 200 and 740 K. Curie temperatures in $\text{Fe}_3\text{O}_4\text{-Mn}_3\text{O}_4$ at different compositions are determined with good agreement between the authors.^[101-106]

Nölle^[107] measured the phase boundary between liquid oxide and halite at 1823 K. The phase boundary between liquid oxide and spinel has been measured by Muan and Somiya.^[84] A number of studies report the solubility of oxygen in liquid Fe-Mn alloys at 1873 K,^[52,84,108-114] with a wide scatter in the different data.

8. Optimization and Results

The optimization of the parameters was performed using the PARROT module of the Thermo-Calc software.^[115] The values for the interaction parameters assessed in this work are listed in Table 2. Data for the pure elements were taken from Dinsdale.^[116]

8.1 Mn-O

The descriptions of all phases in Mn-O from Grundy et al.^[11] except the liquid, α - and $\beta\text{-Mn}_3\text{O}_4$ are unchanged. The calculated phase diagram is shown in Fig. 1.

$\alpha\text{-Mn}_3\text{O}_4$ is known to be a normal spinel^[19,20,117] with Mn^{2+} occupying the tetrahedral sites and Mn^{3+} occupying the octahedral sites. Some interchange between the sites will however occur. The calculated stabilization energies from Dunitz and Orgel^[22] were used to evaluate a parameter to describe the cation distribution between tetrahedral and octahedral sites. The cation distribution for $\beta\text{-Mn}_3\text{O}_4$ is consistent with experiments from Dorris and Mason.^[19]

The investigation on the nonstoichiometry of α - and $\beta\text{-Mn}_3\text{O}_4$ from Keller and Dieckmann^[30] was then used to evaluate the two parameters in each phase describing the deviation from stoichiometry towards lower and higher oxygen contents by formation of cation interstitials and octahedral vacancies. The assessed heat capacity from Grundy et al.^[11] was kept, but the enthalpy of formation and entropy at 298.15 K needed to be adjusted in order to fit the nonstoichiometry data, the enthalpy of the $\alpha\text{-Mn}_3\text{O}_4/\beta\text{-Mn}_3\text{O}_4$ transformation and the transition temperature. The enthalpy of formation, the entropy at 298.15 K and the enthalpy of the $\alpha\text{-Mn}_3\text{O}_4/\beta\text{-Mn}_3\text{O}_4$ transformation from literature are compared to this assessment in Table 1. The magnetic transition temperature was fixed to the experimental value of 43.15 K measured by Chhor et al.^[65]

In Fig. 2 the enthalpy of $\alpha\text{-Mn}_3\text{O}_4$ is plotted against experimental data. The calculated oxygen potential inside the two spinel phases is shown in Fig. 3 and 4.

The liquid parameters for the Mn-O system using the $\text{MnO}_{1.5}$ species instead of the Mn^{3+} species, are obtained from the previous description without any reassessment using

$$^\circ G_{\text{MnO}_{1.5}} = 0.5^\circ G_{\text{Mn}^{3+};\text{O}^{2-}} \quad (\text{Eq 30})$$

$$L_{\text{Mn}^{2+};\text{O}^{2-};\text{MnO}_{1.5}} = L_{\text{Mn}^{2+};\text{Mn}^{3+};\text{O}^{2-}} \quad (\text{Eq 31})$$

Equivalent to the Fe-O system, an additional parameter, $L_{\text{Mn}^{2+};\text{Va}^{2-};\text{MnO}_{1.5}}$, was introduced and optimized to obtain an almost identical fit to the phase diagram as the previous model using Mn^{3+} .

8.2 Fe-Mn-O

Data for the Fe-Mn and Fe-O systems were taken from existing assessments from Huang^[12] and Sundman^[8] (modified by Selleby and Sundman,^[9] Kowalski and Spencer,^[10] Kjellqvist et al.^[11]) respectively.

When optimizing the cubic spinel phase, the parameter $^\circ G_{\text{Mn}^{2+};\text{Fe}^{3+}}$ is first determined against the enthalpy of formation, $\Delta_f^\circ H_{298}$,^[62] the entropy at 298.15 K, $^\circ S_{298}$,^[62] heat content, $H-H_{298}$,^[100] and heat capacity, c_p ,^[100] for MnFe_2O_4 . The magnetic transition temperature was fixed to the experimental value of 577 K, and the Bohr magneton number, $^\circ\beta$, was used as the optimizing parameter to fit the λ -peak in the heat capacity curve. The enthalpy and heat capacity together with experimental data is shown in Fig. 5 and 6.

Curie temperatures for Fe-Mn-O spinels have been measured and an excess parameter for the Curie temperature between Mn_3O_4 and MnFe_2O_4 is needed to reproduce the correct behavior. The calculated and experimental Curie temperature between Fe_3O_4 and Mn_3O_4 is shown in Fig. 7.

Tetragonal MnFe_2O_4 is not stable at normal conditions and the parameter $^\circ G_{\text{Mn}^{2+};\text{Fe}^{3+}}^z$ is used to reproduce the solubility limit of Fe in tetragonal spinel. The calculated phase diagram $\text{Fe}_3\text{O}_4\text{-Mn}_3\text{O}_4$ is shown in Fig. 7.

The distribution of cations between tetrahedral and octahedral sites in MnFe_2O_4 has been studied by a number of authors, with different results. Jiráček and Vratislav^[97] did

Table 2 Assessed parameters (in SI units: J, mole, K)

The magnetic contribution to Gibbs energy is described by:

$$G^{\text{magn}} = RT \ln(\beta + 1) f(\tau), \tau = T/T_C$$

For $\tau < 1$:

$$f(\tau) = 1 - [79\tau^{-1}/140p + 474/497(1/p - 1)(\tau^3/6 + \tau^9/135 + \tau^{15}/600)]/A$$

and for $\tau > 1$:

$$f(\tau) = -(\tau^{-5}/10 + \tau^{-15}/315 + \tau^{-25}/1600)/A$$

where $A = 518/1125 + 11692/15975(1/p - 1)$ and p depends on the structure

Liquid (Fe^{2+} , Mn^{2+})_p(O^{2-} , Va^{0-} , $\text{FeO}_{1.5}$, $\text{MnO}_{1.5}$)_q

$$\begin{aligned} {}^0G_{\text{Fe}^{2+};\text{O}^{2-}} - H_{\text{Fe}}^{\text{SER}} - 2H_{\text{O}}^{\text{SER}} &= 4\text{GFEOLIQ} \\ {}^0G_{\text{Fe}^{2+};\text{Va}} - H_{\text{Fe}}^{\text{SER}} &= \text{GFELIQ} \\ {}^0G_{\text{FeO}_{1.5}} - H_{\text{Fe}}^{\text{SER}} - 1.5H_{\text{O}}^{\text{SER}} &= 2.5\text{GFEOLIQ} - 89819 + 39.962T \\ {}^0G_{\text{Mn}^{2+};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - 2H_{\text{O}}^{\text{SER}} &= 2\text{GMN1O1_L} \\ {}^0G_{\text{Mn}^{2+};\text{Va}} - H_{\text{Mn}}^{\text{SER}} &= \text{GMN_L} \\ {}^0G_{\text{MnO}_{1.5}} - H_{\text{Mn}}^{\text{SER}} - 1.5H_{\text{O}}^{\text{SER}} &= 0.5\text{GMN2O3_L} \\ {}^0L_{\text{Fe}^{2+};\text{O}^{2-};\text{Va}} &= 176681 - 16.368T \\ {}^1L_{\text{Fe}^{2+};\text{O}^{2-};\text{Va}} &= -65655 + 30.869T \\ {}^0L_{\text{Fe}^{2+};\text{O}^{2-};\text{FeO}_{1.5}} &= -26362 \\ {}^1L_{\text{Fe}^{2+};\text{O}^{2-};\text{FeO}_{1.5}} &= 13353 \\ {}^0L_{\text{Fe}^{2+};\text{Va};\text{FeO}_{1.5}} &= 110000 \\ {}^0L_{\text{Mn}^{2+};\text{O}^{2-};\text{Va}} &= 129519 \\ {}^1L_{\text{Mn}^{2+};\text{O}^{2-};\text{Va}} &= -45459 \\ {}^0L_{\text{Mn}^{2+};\text{O}^{2-};\text{MnO}_{1.5}} &= -33859 \\ {}^0L_{\text{Mn}^{2+};\text{Va};\text{MnO}_{1.5}} &= 110000^* \\ {}^0L_{\text{Fe}^{2+};\text{Mn}^{2+};\text{Va}} &= -3950 + 0.489T \\ {}^1L_{\text{Fe}^{2+};\text{Mn}^{2+};\text{Va}} &= 1145 \\ {}^0L_{\text{Fe}^{2+};\text{Mn}^{2+};\text{O}^{2-}} &= -11000^* \\ {}^1L_{\text{Fe}^{2+};\text{Mn}^{2+};\text{O}^{2-}} &= -4700^* \\ {}^0L_{\text{Fe}^{2+};\text{Va};\text{MnO}_{1.5}} &= 110000^* \\ {}^0L_{\text{Mn}^{2+};\text{Va};\text{FeO}_{1.5}} &= 110000^* \\ {}^0L_{\text{Mn}^{2+};\text{O}^{2-};\text{FeO}_{1.5}} &= -47000^* \end{aligned}$$

Halite: (Fe^{2+} , Fe^{3+} , Mn^{2+} , Mn^{3+} , Va)₁(O^{2-})₁

$$\begin{aligned} {}^0G_{\text{Fe}^{2+};\text{O}^{2-}} - H_{\text{Fe}}^{\text{SER}} - H_{\text{O}}^{\text{SER}} &= \text{GWUSTITE} \\ {}^0G_{\text{Fe}^{3+};\text{O}^{2-}} - H_{\text{Fe}}^{\text{SER}} - H_{\text{O}}^{\text{SER}} &= 1.25\text{AWUSTITE} + 1.25\text{GWUSTITE} \\ {}^0G_{\text{Mn}^{2+};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - H_{\text{O}}^{\text{SER}} &= \text{GMN1O1} \\ {}^0G_{\text{Mn}^{3+};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - H_{\text{O}}^{\text{SER}} &= \text{GMN1O1} - 21884 - 22.185T \\ {}^0G_{\text{Va};\text{O}^{2-}} - H_{\text{O}}^{\text{SER}} &= 0 \\ {}^0L_{\text{Fe}^{2+};\text{Fe}^{3+};\text{O}^{2-}} &= -12324.4 \\ {}^1L_{\text{Fe}^{2+};\text{Fe}^{3+};\text{O}^{2-}} &= 20070 \\ {}^0L_{\text{Mn}^{2+};\text{Mn}^{3+};\text{O}^{2-}} &= -42105 \\ {}^1L_{\text{Mn}^{2+};\text{Mn}^{3+};\text{O}^{2-}} &= 46513 \\ {}^0L_{\text{Fe}^{2+};\text{Mn}^{2+};\text{O}^{2-}} &= -1300^* \\ {}^0L_{\text{Fe}^{3+};\text{Mn}^{2+};\text{O}^{2-}} &= 11000^* \\ {}^1L_{\text{Fe}^{3+};\text{Mn}^{2+};\text{O}^{2-}} &= -28000^* \\ {}^0L_{\text{Fe}^{3+};\text{Mn}^{3+};\text{O}^{2-}} &= -23000 + 33T^* \end{aligned}$$

Corundum: (Fe^{2+} , Fe^{3+} , Mn^{3+})₂(Fe^{3+} , Va)₁(O^{2-})₃

$$\begin{aligned} {}^0G_{\text{Fe}^{2+};\text{Fe}^{3+};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} &= \text{GFE2O3} + 85000 \\ {}^0G_{\text{Fe}^{3+};\text{Fe}^{3+};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} &= \text{GFE2O3} + 85000 \\ {}^0G_{\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - 2H_{\text{Fe}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} &= \text{GFE2O3} \\ {}^0G_{\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - 2H_{\text{Fe}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} &= \text{GFE2O3} \\ {}^0G_{\text{Mn}^{3+};\text{Fe}^{3+};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} &= \text{GMN2O3} + 110500 - 3.7T^* \\ {}^0G_{\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} &= \text{GMN2O3} + 25500 - 3.7T^* \end{aligned}$$

Section I: Basic and Applied Research

Table 2 continued

Magnetic properties ($p = 0.28$):

for compounds containing Fe cations on the first sublattice $T_C = -2867$ and $\beta = -25.1$

for compounds containing Mn cations on the first sublattice $T_C = 0$ and $\beta = 0$

Bixbyite: $(\text{Fe}^{3+}, \text{Mn}^{3+})_2(\text{O}^{2-})_3$

$${}^{\circ}G_{\text{Fe}^{3+};\text{O}^{2-}} - 2H_{\text{Fe}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} = \text{GFE2O3} + 18000 - 10T^*$$

$${}^{\circ}G_{\text{Mn}^{3+};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - 3H_{\text{O}}^{\text{SER}} = \text{GMN2O3}$$

$${}^{\circ}L_{\text{Fe}^{3+}, \text{Mn}^{3+}; \text{O}^{2-}} = 1500^*$$

Pyrolusite: $(\text{MnO}_2): (\text{Mn}^{4+})_1(\text{O}^{2-})_2$

$${}^{\circ}G_{\text{Mn}^{4+};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 2H_{\text{O}}^{\text{SER}} = -545091 + 395.379T - 65.277T \ln(T) - 0.007803T^2 + 664955/T - 0.007803T^2 + 664955/T$$

β -Spinel: $(\text{Fe}^{2+}, \text{Fe}^{3+}, \text{Mn}^{2+})_1(\text{Fe}^{2+}, \text{Fe}^{3+}, \text{Mn}^{2+}, \text{Mn}^{3+}, \text{Mn}^{4+}, \text{Va})_2(\text{Fe}^{2+}, \text{Mn}^{2+}, \text{Va})_2(\text{O}^{2-})_4$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB} + \text{JFF}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB}$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB} - \text{JFF}$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Va};\text{Va};\text{O}^{2-}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 5\text{GFFB} + \text{C}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Va};\text{Va};\text{O}^{2-}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 5\text{GFFB} - \text{JFF} + \text{C}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Mn}^{2+};\text{Va};\text{O}^{2-}} - 3H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = \text{GM2M2B}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 3H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GMMB}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Mn}^{4+};\text{Va};\text{O}^{2-}} - 3H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 14\text{GMMB} + \text{JM} - \text{GM2M2B}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Va};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 8\text{GGMN2O3B} - 56\text{GMMB} - 3\text{JM} + 3\text{GM2M2B} + 2RT(6 \ln(6) - 3 \ln(3) - 2 \ln(2))$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Mn}^{2+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB} - 7\text{GMFB} + \text{GM2M2B}$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFMB}$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Mn}^{4+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 28\text{GFMB} + 2\text{JFMB} - 14\text{GMMB} - 7\text{GFFB} + \text{JFF}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Mn}^{2+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB} - \text{JFF} - 7\text{GMFB} + \text{GM2M2B}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB} - \text{JFF} + 7\text{GMMB} - 7\text{GMFB}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Mn}^{4+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFB} - \text{JFF} + 14\text{GMMB} + \text{JM} - 7\text{GMFB} - \text{GM2M2B}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 2H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 14\text{GFMB} - 14\text{GMMB} - \text{JM} + 2\text{JFMB} + \text{GM2M2B}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 2H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GMFB}$$

$${}^{\circ}G_{*};\text{Fe}^{2+};\text{O}^{2-} = {}^{\circ}G_{*};\text{Va};\text{O}^{2-} + 2\text{GFFB} - \text{JFF} + \text{D}$$

$${}^{\circ}G_{*};\text{Mn}^{2+};\text{O}^{2-} = {}^{\circ}G_{*};\text{Va};\text{O}^{2-} + 8\text{GGMN1O1B} - 2\text{GM2M2B} + 4RT \ln(2)$$

Magnetic properties ($p = 0.28$):

for compounds containing only Fe cations $T_C = 848$ and $\beta = 44.54$

for compounds containing only Mn cations $T_C = 43.15^*$ and $\beta = 0^*$

for compounds containing Fe + Mn cations $T_C = 577^*$ and $\beta = 6^*$

$${}^{\circ}\beta_{\text{Mn}^{2+};\text{Fe}^{3+}, \text{Mn}^{3+}; \text{Va}; \text{O}^{2-}} = 450^*$$

α -Spinel: $(\text{Fe}^{2+}, \text{Fe}^{3+}, \text{Mn}^{2+}, \text{Mn}^{3+})_1(\text{Fe}^{2+}, \text{Fe}^{3+}, \text{Mn}^{2+}, \text{Mn}^{3+}, \text{Va})_2(\text{Fe}^{2+}, \text{Mn}^{2+}, \text{Va})_2(\text{O}^{2-})_4$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFA} + \text{JFF}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFA}$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFA}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - 3H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFA} - \text{JFF}$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Va};\text{Va};\text{O}^{2-}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 5\text{GFFA} + \text{C}$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Va};\text{Va};\text{O}^{2-}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 5\text{GFFA} - \text{JFF} + \text{C}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Mn}^{2+};\text{Va};\text{O}^{2-}} - 3H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 21\text{GMMA} + 2\text{JMMA} - 2\text{GM3M3A}$$

$${}^{\circ}G_{\text{Mn}^{3+};\text{Mn}^{2+};\text{Va};\text{O}^{2-}} - 3H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 14\text{GMMA} + 2\text{JMMA} - \text{GM3M3A}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 3H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GMMA}$$

$${}^{\circ}G_{\text{Mn}^{3+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 3H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = \text{GM3M3A}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Va};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 8\text{GGMN2O3A} - 6\text{GM3M3A} + 7\text{GMMA} + 2RT(6 \ln(6) - 5 \ln(5))$$

$${}^{\circ}G_{\text{Mn}^{3+};\text{Va};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 8\text{GGMN2O3A} - 5\text{GM3M3A} + 2RT(6 \ln(6) - 5 \ln(5))$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Mn}^{2+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFMA} + 14\text{GMMA} + 2\text{JMMA} - 2\text{GM3M3A} + 4RT \ln(2)$$

$${}^{\circ}G_{\text{Fe}^{2+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFMA}$$

Table 2 continued

$${}^{\circ}G_{\text{Fe}^{3+};\text{Mn}^{2+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 21\text{GMMA} + 2\text{JMMA} + 7\text{GFFA} - \text{JFF} - 7\text{GMFA} - 2\text{GM3M3A} + 4RT \ln(2)$$

$${}^{\circ}G_{\text{Fe}^{3+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} - 2H_{\text{Mn}}^{\text{SER}} - H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFMA} - \text{JFF}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 2H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFA} + \text{JFF} + 7\text{GMMA} - 7\text{GFMA}$$

$${}^{\circ}G_{\text{Mn}^{2+};\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 2H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GMFA}$$

$${}^{\circ}G_{\text{Mn}^{3+};\text{Fe}^{2+};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 2H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFA} + \text{JFF} - 7\text{GFMA} + \text{GM3M3A}$$

$${}^{\circ}G_{\text{Mn}^{3+};\text{Fe}^{3+};\text{Va};\text{O}^{2-}} - H_{\text{Mn}}^{\text{SER}} - 2H_{\text{Fe}}^{\text{SER}} - 4H_{\text{O}}^{\text{SER}} = 7\text{GFFA} - 7\text{GFMA} + \text{GM3M3A}$$

$${}^{\circ}G_{*};\text{Fe}^{2+};\text{O}^{2-} = {}^{\circ}G_{*};\text{Va};\text{O}^{2-} + 2\text{GFFA} - \text{JFF} + \text{D}$$

$${}^{\circ}G_{*};\text{Mn}^{2+};\text{O}^{2-} = {}^{\circ}G_{*};\text{Va};\text{O}^{2-} + 8\text{GGMN1O1A} - 42\text{GMMA} - 4\text{JMMA} + 4\text{GM3M3A} + 4RT \ln(2)$$

Magnetic properties ($p = 0.28$):

for compounds containing only Fe cations $T_C = 848$ and $\beta = 44.54$

for compounds containing only Mn cations $T_C = 43.15^*$ and $\beta = 0^*$

for compounds containing Fe + Mn cations $T_C = 577^*$ and $\beta = 6^*$

$${}^{\circ}\beta_{\text{Mn}^{2+};\text{Fe}^{3+};\text{Mn}^{3+};\text{Va};\text{O}^{2-}} = 450^*$$

Functions

$$\text{GFELIQ} (298.15 < T < 1811) = 12040.17 - 6.55843T - 3.6751551E-21T^7 + \text{GHSERFE}$$

$$\text{GFELIQ} (1811 < T < 6000) = -10838.83 + 291.302T - 46T \ln(T)$$

$$\text{GFEOLIQ} = -137252 + 224.641T - 37.1815T \ln(T)$$

$$\text{GMN_L} (298.15 < T < 1519) = \text{GHSERMN} + 17859.91 - 12.6208T - 4.41929E-21T^7$$

$$\text{GMN_L} (1519 < T < 6000) = \text{GHSERMN} + 18739.51 - 13.2288T - 1.656847E+30T^{-9}$$

$$\text{GMN1O1_L} = \text{GMN1O1} + 43947 - 20.628T$$

$$\text{GMN1O1} = -402478 + 259.356T - 46.835T \ln(T) - .00385T^2 + 212922/T$$

$$\text{GMN2O3_L} = +2\text{GMN1O1} + 0.5\text{GO2GAS} - 64953 + 43.144T$$

$$\text{GHSERMN} (298.15 < T < 1519) = -8115.28 + 130.059T - 23.4582T \ln(T) - 0.00734768T^2 + 69827.1/T$$

$$\text{GHSERMN} (1519 < T < 6000) = -28733.41 + 312.2648T - 48T \ln(T) + 1.656847E+30/T^9$$

$$\text{GHSERFE} (298.15 < T < 1811) = 1225.7 + 124.134T - 23.5143T \ln(T) - 0.00439752T^2 - 5.8927E-08T^3 + 77359/T$$

$$\text{GHSERFE} (1811 < T < 6000) = -25383.581 + 299.31255T - 46T \ln(T) + 2.29603E+31/T^9$$

$$\text{GO2GAS} (298.15 < T < 1000) = -6961.74451 - 51.0057202T - 22.2710136T \ln(T) - 0.0101977469T^2 + 1.32369208E-06T^3 - 76729.7484/T$$

$$\text{GO2GAS} (1000 < T < 3300) = -13137.5203 + 25.3200332T - 33.627603T \ln(T) - 0.00119159274T^2 + 1.35611111E-08T^3 + 525809.556/T$$

$$\text{GO2GAS} (3300 < T < 6000) = -27973.4908 + 62.5195726T - 37.9072074T \ln(T) - 8.50483772E-04T^2 + 2.14409777E-08T^3 + 8766421.4/T$$

$$\text{AWUSTITE} = -55384 + 27.888T$$

$$\text{GWUSTITE} = -279318 + 252.848T - 46.12826T \ln(T) - 0.0057402984T^2$$

$$\text{GFE2O3} = -858683 + 827.946T - 137.0089T \ln(T) + 1453810/T$$

$$\text{GMN2O3} = -998618 + 588.619T - 101.956T \ln(T) - .018844T^2 + 589055/T$$

$$\text{JFF} = 46826 - 27.266T$$

$$\text{C} = 120730 - 20.102T$$

$$\text{D} = 402520 - 30.529T$$

$$\text{GFFB} = -161731 + 144.873T - 24.9879T \ln(T) - 0.0011952256T^2 + 206520/T$$

$$\text{GFMB} = \text{GMN2O3}/7 + \text{GWUSTITE}/7^*$$

$$\text{GMFB} = -182450 + 133T - 23.099T \ln(T) - 0.00147T^2 + 124000/T^*$$

$$\text{GMMB} = \text{GMN3O4B}/7 + \text{GMN3O4A}/7^*$$

$$\text{GMN3O4A} = -1439700 + 892.2T - 154.748T \ln(T) - 0.017408T^2 + 986139/T^*$$

$$\text{GMN3O4B} = 15270 + 7T^*$$

$$\text{JMMA} = 26210 - 17.46T^*$$

$$\text{JMFB} = 28000^*$$

$$\text{JFMB} = -27000^*$$

$$\text{GGMN1O1B} = \text{GMN1O1} + 41500 - 10.25T^*$$

$$\text{GGMN2O3B} = \text{GMN2O3} + 192300 - 193.8T + 0.05T^2^*$$

$$\text{GM2M2B} = 21\text{GMFB} + 2\text{JMFB} - 14\text{GFFB} + 2\text{JFF}^*$$

$$\text{GFFA} = \text{GFFB} + 1000$$

$$\text{GFMA} = \text{GFMB}^*$$

$$\text{GMFA} = \text{GMFB} + 4900 - 1.9T^*$$

$$\text{GMMA} = \text{GMN3O4A}/7^*$$

$$\text{JMMA} = 95000^*$$

$$\text{JMFA} = 28000^*$$

Table 2 continued

$$\text{GGMN1O1A} = \text{GMN1O1} + 58500 - 117^*$$

$$\text{GGMN2O3A} = \text{GMN2O3} + 240000 - 211.87 + 0.057^*x^2$$

$$\text{GM3M3A} = 10.5\text{GMMA} + \text{JMMA} - 10.5\text{GMFA} - \text{JMFA} + 7\text{GFFA} - \text{JFF}^*$$

* indicates parameters assessed in this work

Parameters for the metallic phases and the gas phase can be found elsewhere^[10,12,116]

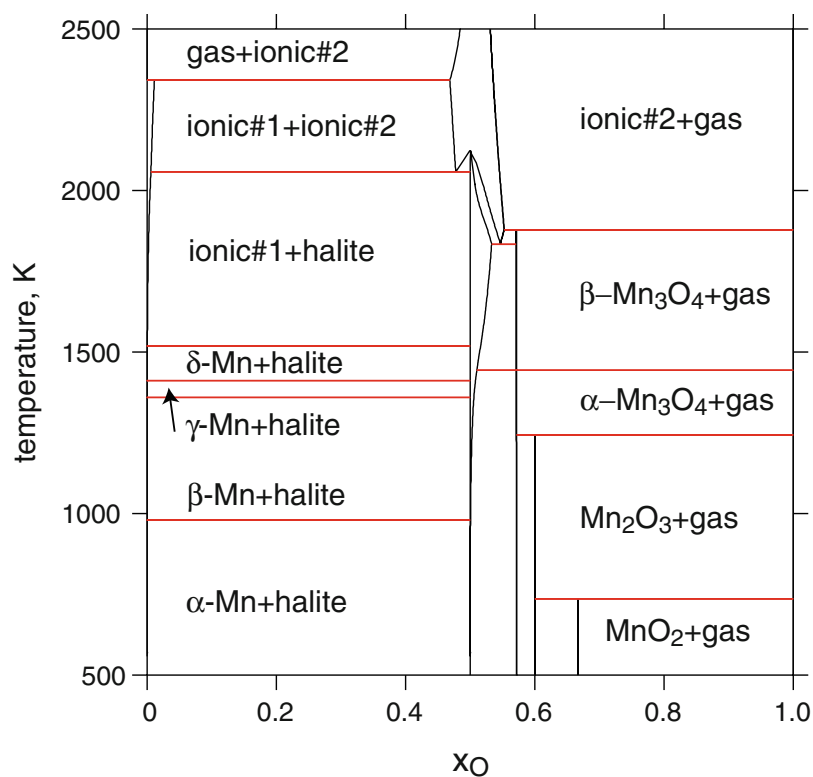


Fig. 1 Calculated Mn-O phase diagram at 1 atmosphere total pressure

neutron diffraction investigations at elevated temperatures between 603 and 1443 K. Hasting and Corliss^[93] found the degree of inversion to be independent of preparation conditions and temperature. Other authors found a very low degree of inversion.^[118,119] Faller and Birchenall^[120] showed that in some cases even rapid quenching is not sufficient to retain the equilibrium distribution of cations corresponding to the annealing temperature. Therefore, the experimental data on the degree of inversion (fraction of Mn ions in octahedral sites) from Jiráček and Vratislav was used to evaluate the cation distribution in MnFe_2O_4 . MnFe_2O_4 is known to be an almost normal spinel at room temperature with Mn^{2+} ions on tetrahedral sites and Fe^{3+} ions on octahedral sites. At increasing temperature the degree of inversion increases. The distribution of cations is determined by the formula $\text{Mn}_{1-\lambda}\text{Fe}_\lambda[\text{Mn}_\lambda\text{Fe}_{2-\lambda}]\text{O}_4$, where the cations inside the square brackets are in

octahedral sites while the cations in front of the brackets are in tetrahedral sites. The calculated degree of inversion is shown in Fig. 8. The calculated cation distribution in cubic $\text{Fe}_{3-x}\text{Mn}_x\text{O}_4$ at 1000 K is shown in Fig. 9, where the tetragonal spinel phase was excluded in the calculation. Terayama et al.^[100] found a wide nonstoichiometric range in MnFe_2O_4 at 1153 K, corresponding to $-0.2258 \leq \delta \leq 0$ in $(\text{Fe}_x\text{Mn}_{1-x})_{3-\delta}\text{O}_4$. This huge deviation from stoichiometry seems very unlikely and disagrees with the measurements from Bulgakova and Rozanov,^[74] whose results agree well with our calculated values, even though they were not taken into account in this optimization, see Fig. 10.

The nonstoichiometry of $(\text{Fe}_{1-x}\text{Mn}_x)_{1-\delta}\text{O}$ at 1273 and 1473 K for different values on x , investigated by Subramanian and Dieckmann^[72] and Franke and Dieckmann,^[69] were used to optimize the interaction parameters in halite.

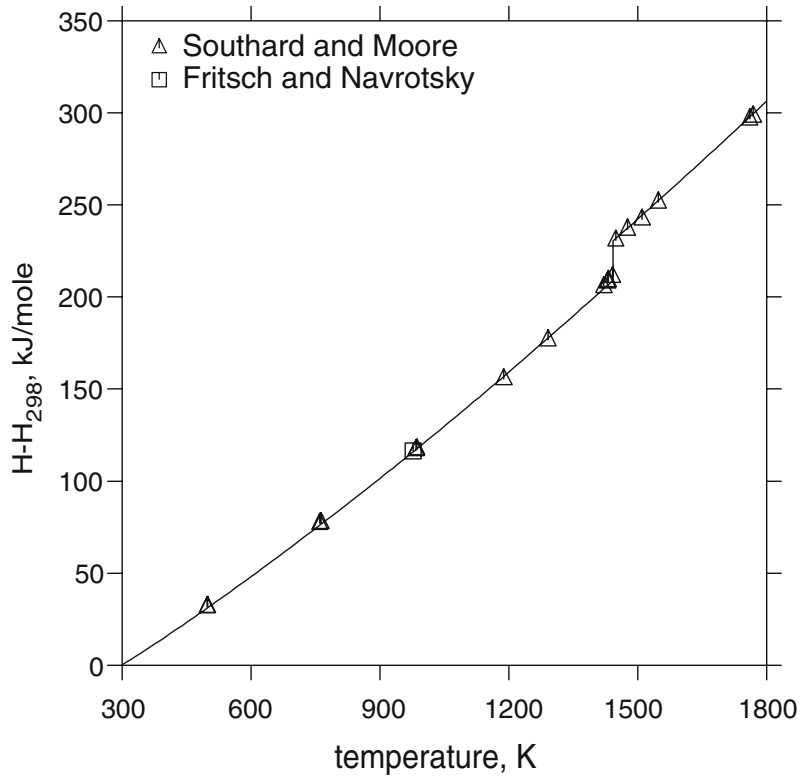


Fig. 2 Calculated and experimental^[28,66] enthalpy of Mn_3O_4

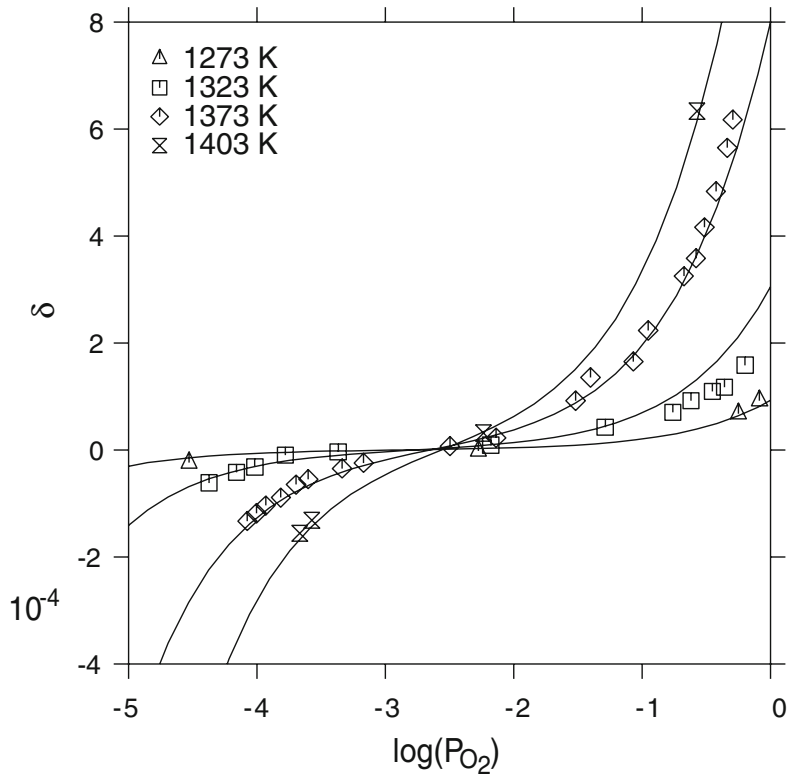


Fig. 3 Calculated and experimental^[30] oxygen potential in $\alpha\text{-}Mn_{3-\delta}O_4$

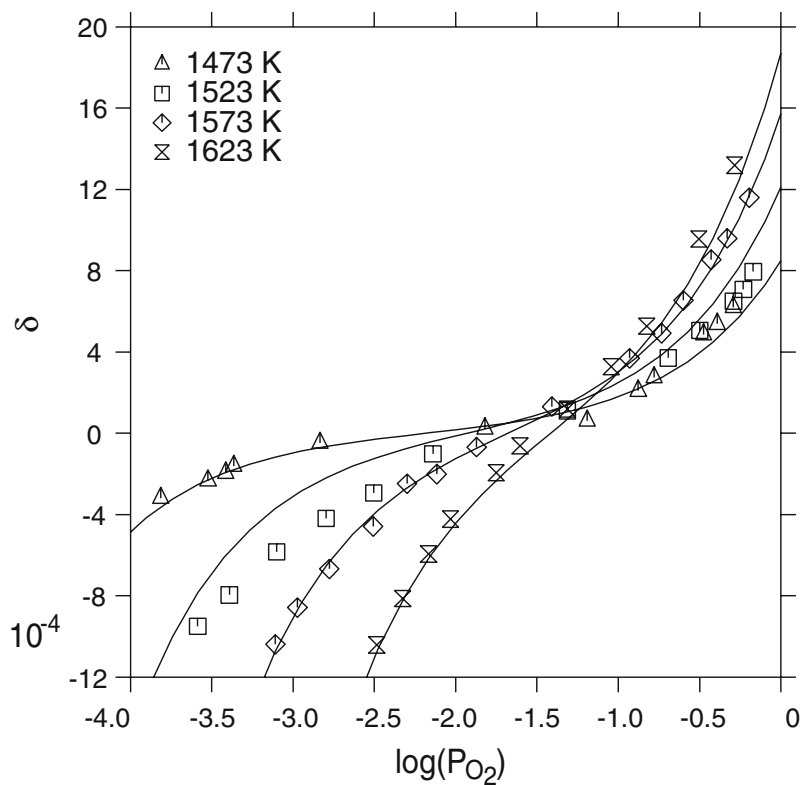


Fig. 4 Calculated and experimental^[30] oxygen potential in $\beta\text{-Mn}_{3-\delta}\text{O}_4$

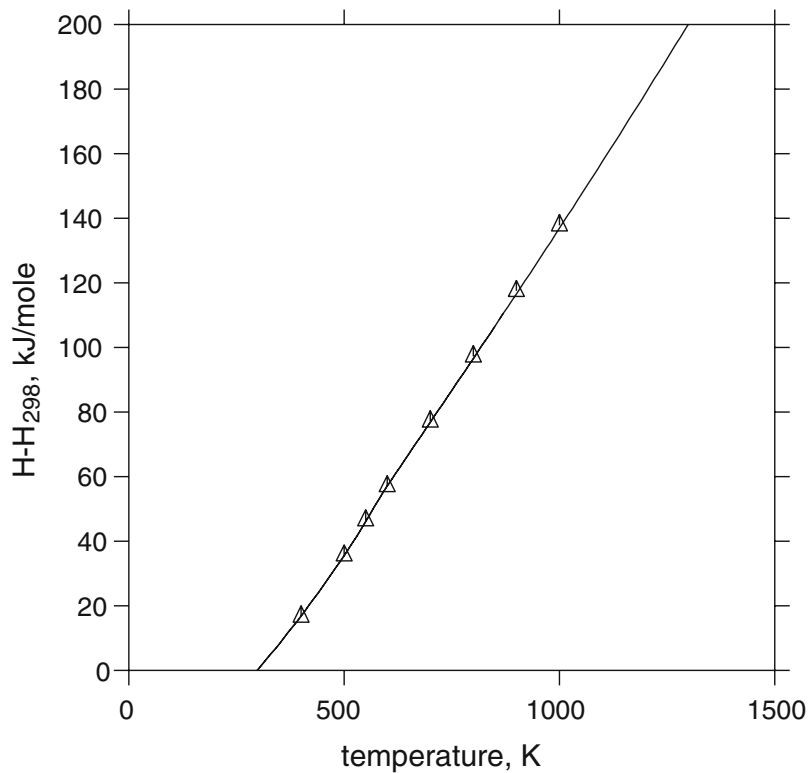


Fig. 5 Calculated and experimental^[101] enthalpy of MnFe_2O_4

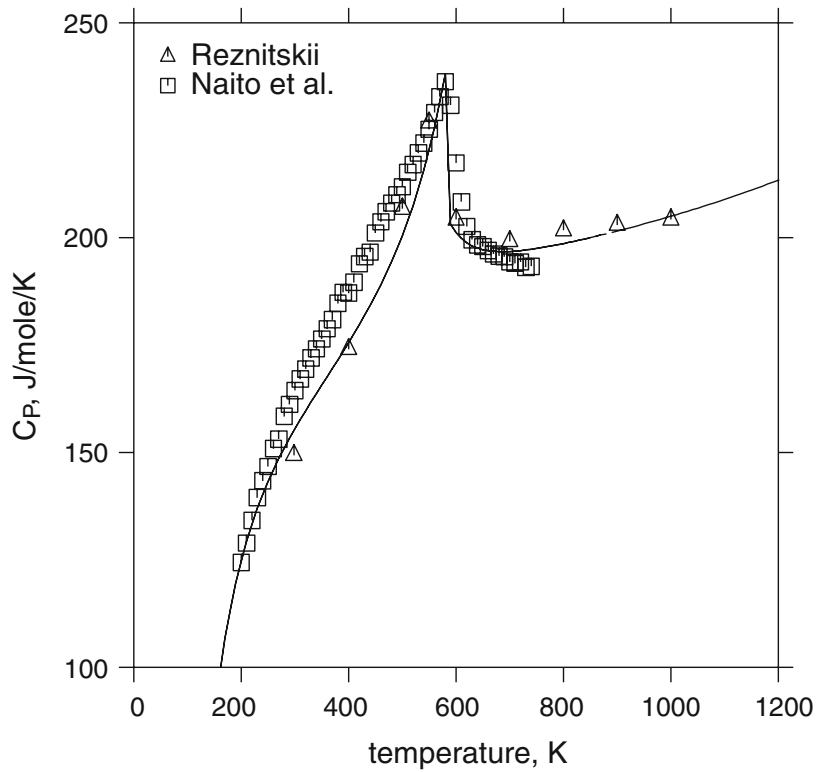


Fig. 6 Calculated and experimental^[101,102] heat capacity of MnFe_2O_4

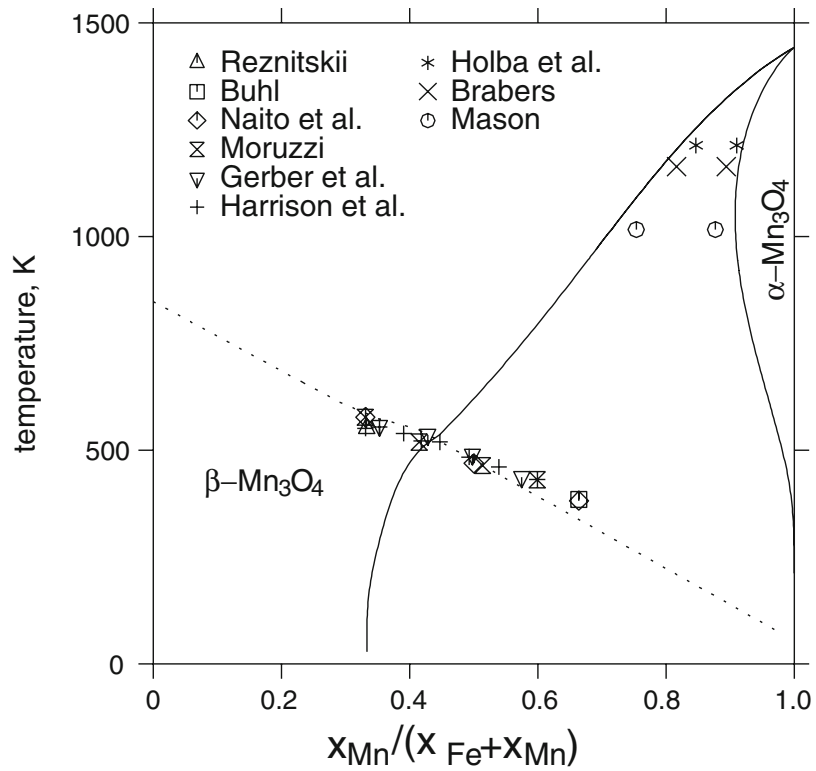


Fig. 7 Calculated and experimental^[89-91,101-106] phase diagram and Curie temperature between Fe_3O_4 and Mn_3O_4

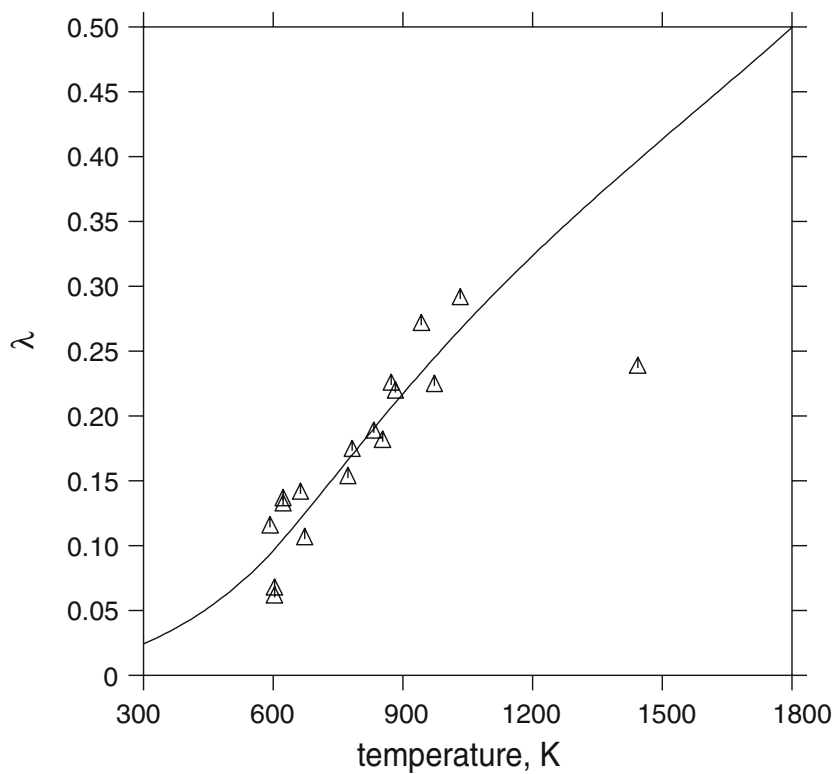


Fig. 8 Calculated and experimental^[97] degree of inversion of MnFe_2O_4 ($\text{Mn}_{1-\lambda}\text{Fe}_\lambda[\text{Mn}_\lambda\text{Fe}_{2-\lambda}]\text{O}_4$)

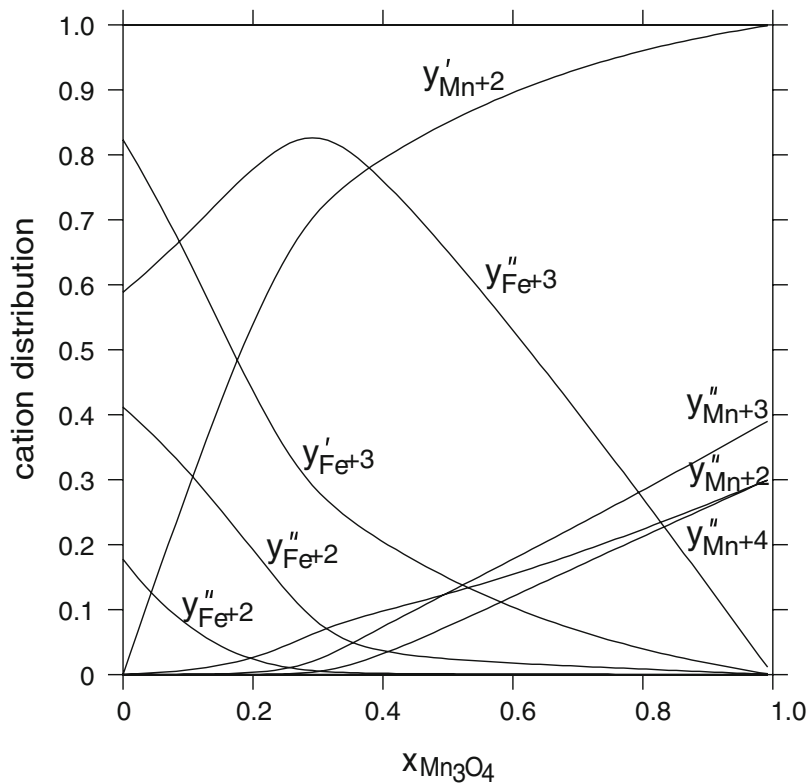


Fig. 9 Calculated cation distribution in cubic Fe_3O_4 - Mn_3O_4 at 1000 K

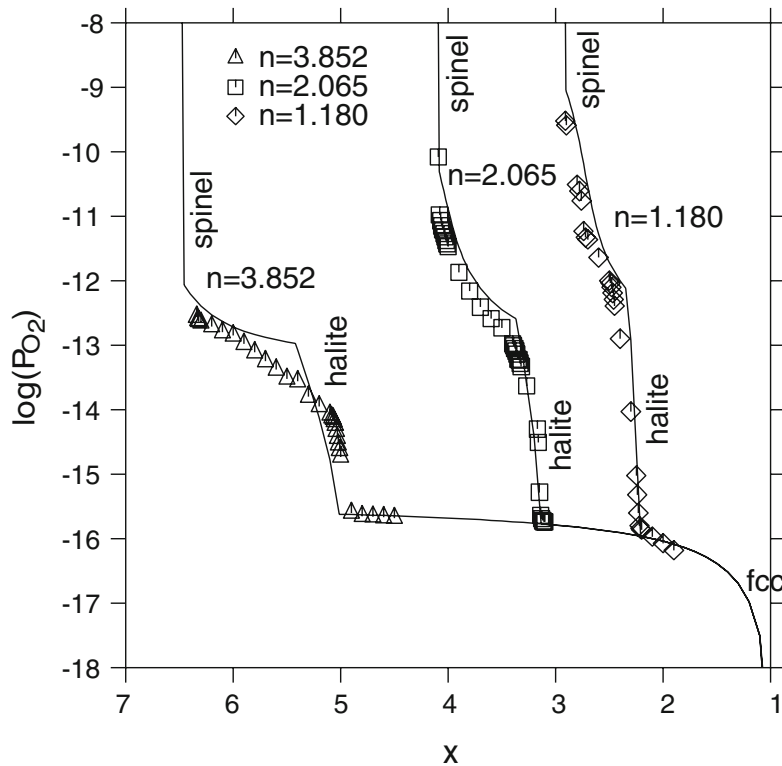


Fig. 10 Calculated and experimental^[74] oxygen potential at 1242 K in MnFe_nO_x .

The calculated partial pressure of oxygen in nonstoichiometric halite is shown in Fig. 11 and 12. It could be noted that the slope of the calculations does not perfectly align with the experiments. To change the slope of the calculated curves, the model for the manganowustite phase needs to be changed to also include Mn^{4+} ions.

When reasonable parameters had been given to the halite and spinel phases, experimental information on invariant equilibria was included in the assessment. Information from Subramanian and Dieckmann,^[72] Franke and Dieckmann^[69] and Schwerdtfeger and Muan^[52] of the two-phase regions of halite/fcc and halite/spinel at two temperatures (1273 and 1473 K) were used to further improve the description of halite and spinel. Figure 13 shows the calculated composition-oxygen activity phase diagram at 1273 K together with experimental data.

The investigations of the two-phase regions of corundum/bixbyite and corundum/spinel from Ref 69, 75, 84, 86, 121 were used to describe the solubility of Mn in Fe_2O_3 . The data from Bergstein and Kleinert^[85] on the β -spinel/corundum phase boundary at 1273 K could not be reproduced. To correctly describe the solubility of Fe in Mn_2O_3 , an excess parameter was required to be able to reproduce the experimental data. A phase diagram calculated in air ($P = 0.21$ bar) is shown in Fig. 14 together with experimental data.

The liquid phase is optimized using the data from Muan and Somiya^[84] and Nölle^[107] on the phase boundaries

between liquid oxide and spinel/halite respectively. The experiments on the solubility of oxygen in the metallic melt are not taken into consideration in this assessment due to the large scattering. The experimental and calculated oxygen content of the metallic liquid in equilibrium with the halite phase are shown in Fig. 15.

Calculated isothermal sections at two different temperatures are shown in Fig. 16 and 17.

9. Conclusions and Discussion

The present assessment gives a good description of the available experimental information in the ternary Fe-Mn-O system. A complete list of all parameters is found in Table 2. Part of the Mn-O system has been revised. In the liquid phase the Mn^{3+} ion has been replaced by a neutral $\text{MnO}_{1.5}$ species equivalent to the Fe-O system. The spinel phases (α - and β - Mn_3O_4) are here modelled using a more complex description than the previous assessment from Grundy et al.^[11] The new model describes the cation distribution of ions between tetrahedral and octahedral sites and the nonstoichiometry of the phases. The description of the spinel phases in the Fe-Mn-O system is consistent with the description of the Fe-Cr-Ni-O spinel from an earlier work,^[11] but to be able to do thermodynamic calculations in the Fe-Cr-Mn-Ni-O system the Cr-Mn-O and Mn-Ni-O

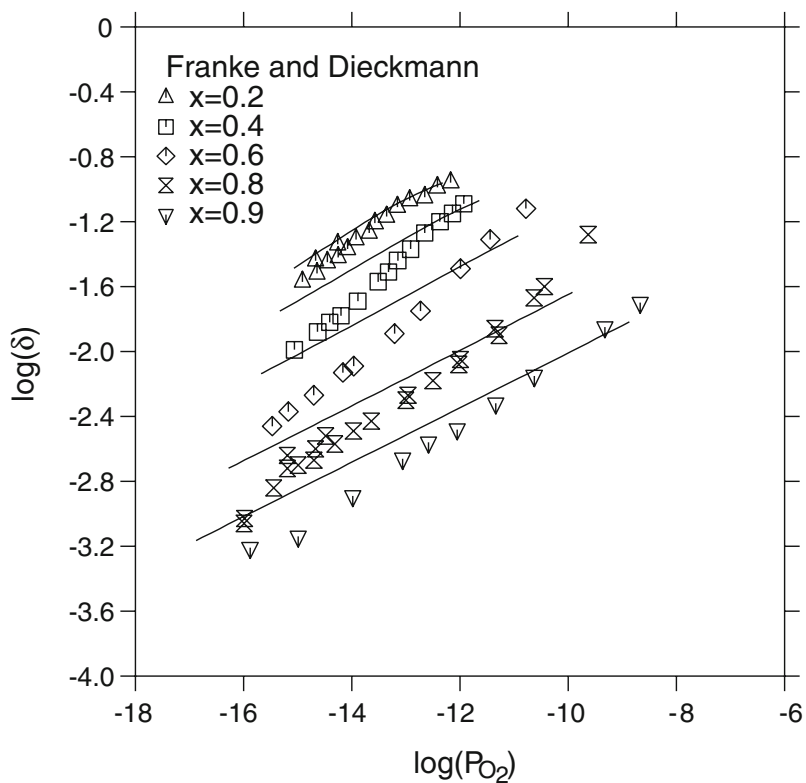


Fig. 11 Calculated and experimental^[69] oxygen potential in $(\text{Fe}_{1-x}\text{Mn}_x)_{1-\delta}\text{O}$ at 1273 K

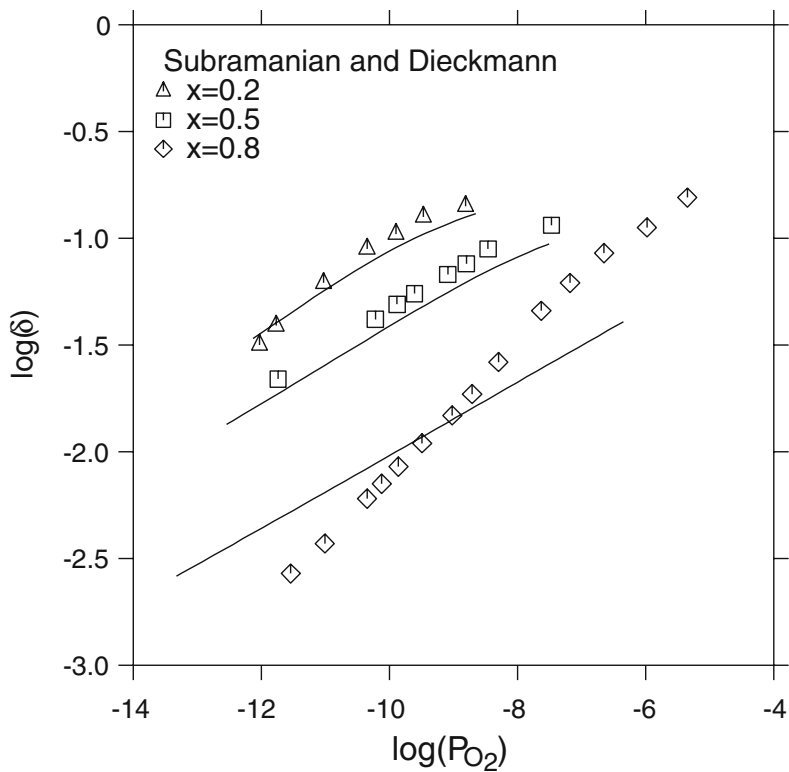


Fig. 12 Calculated and experimental^[72] oxygen potential in $(\text{Fe}_{1-x}\text{Mn}_x)_{1-\delta}\text{O}$ at 1473 K

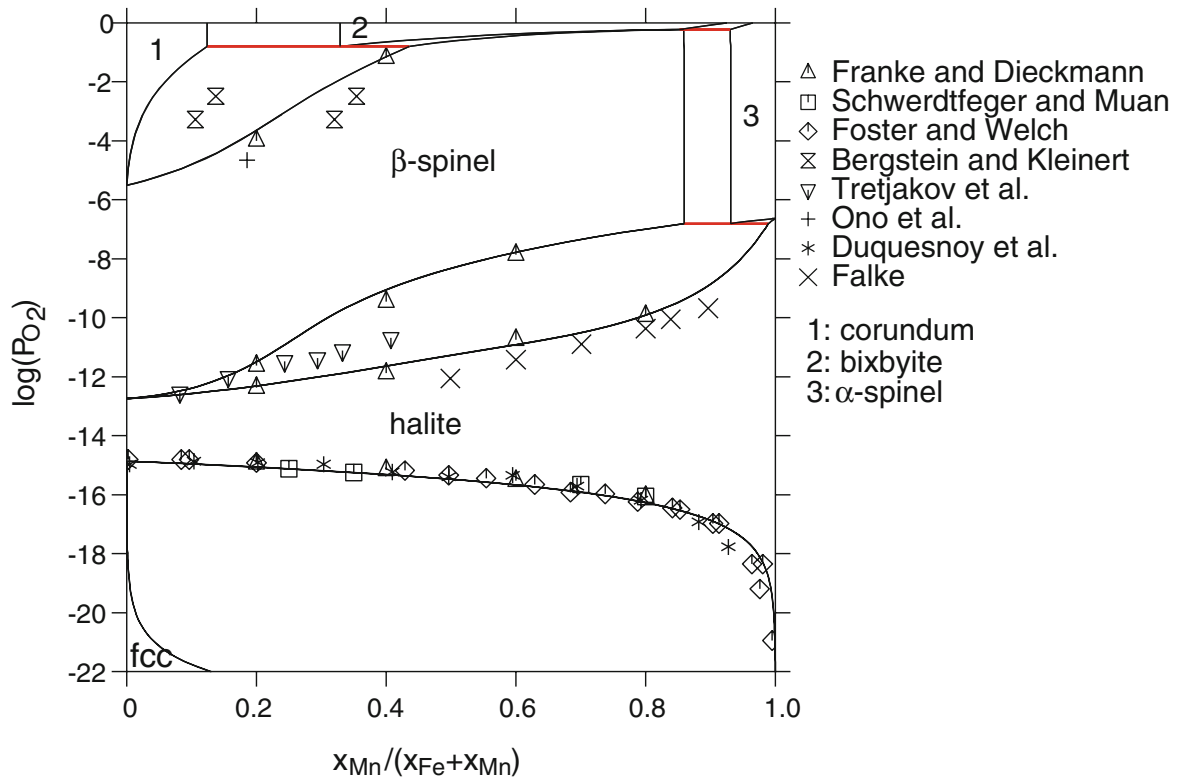


Fig. 13 Calculated and experimental^[52,69,73,75-77,85,121] phase diagram at 1273 K

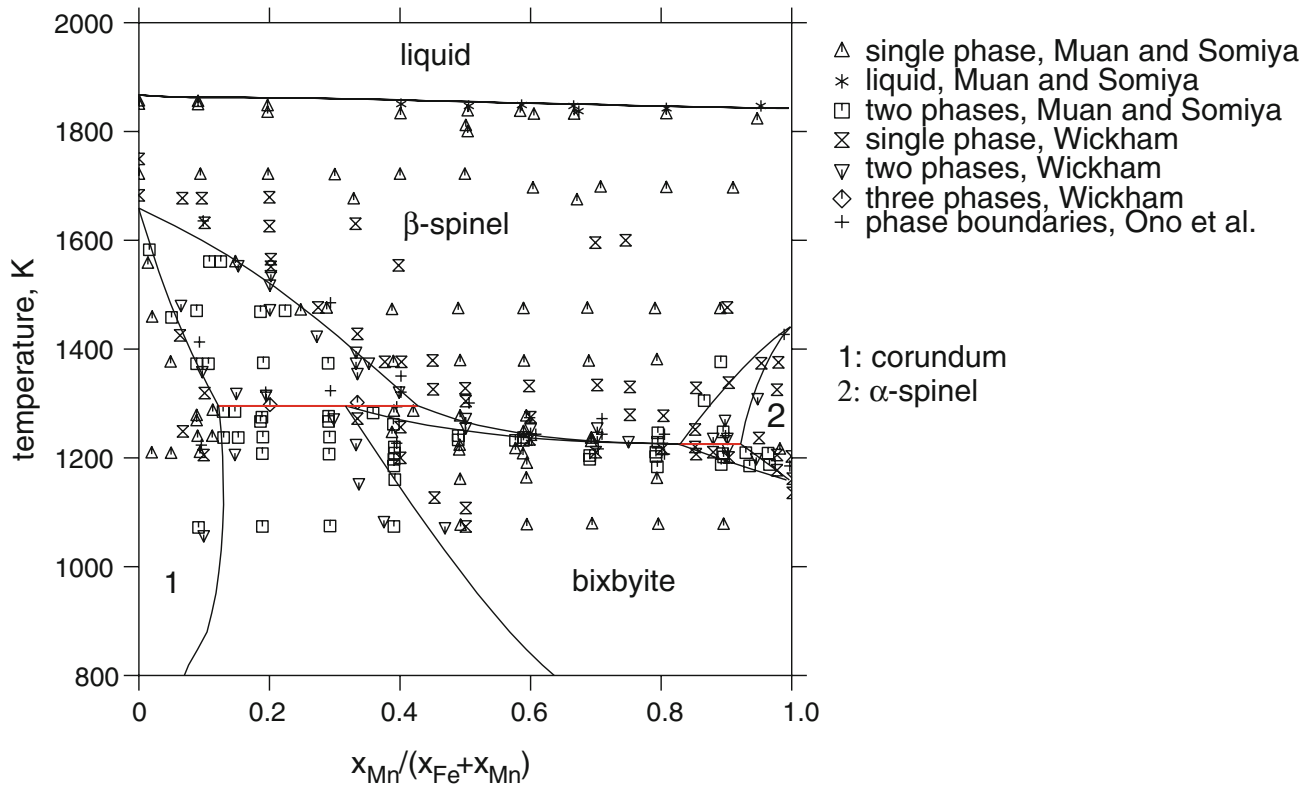


Fig. 14 Calculated and experimental^[75,84,86] phase diagram for a fixed oxygen partial pressure of 0.21 bar

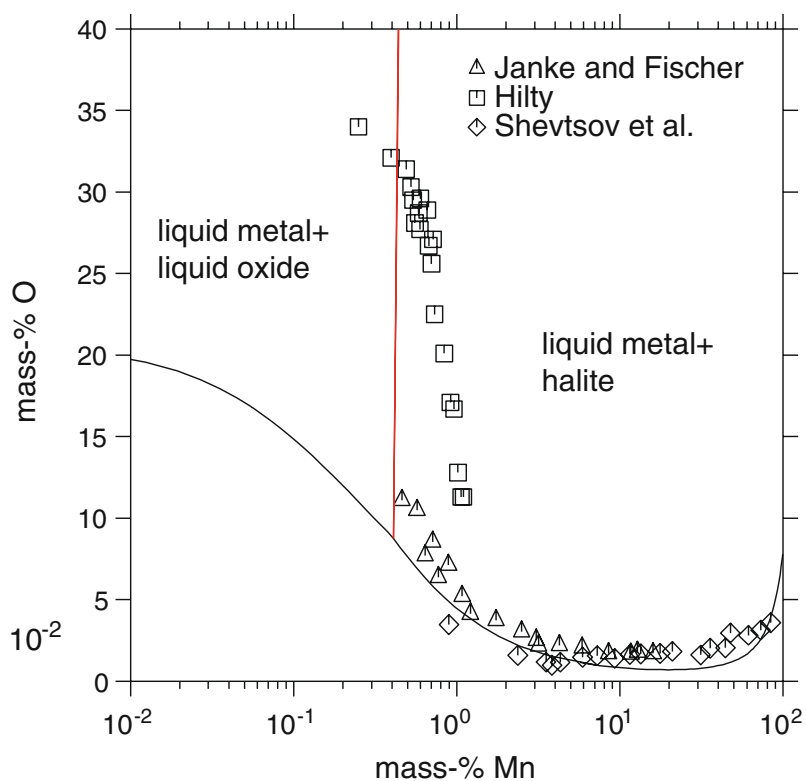


Fig. 15 Calculated and experimental^[108,109,112] oxygen solubility in liquid Fe-Mn in equilibrium with halite and liquid oxide at 1873 K

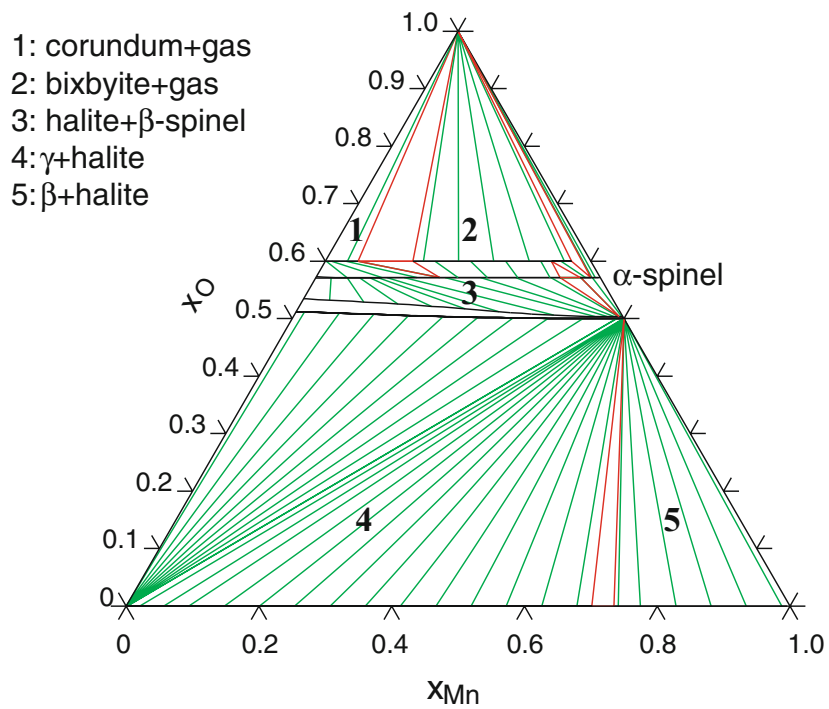


Fig. 16 Calculated isothermal section of the Fe-Mn-O system at 1273 K

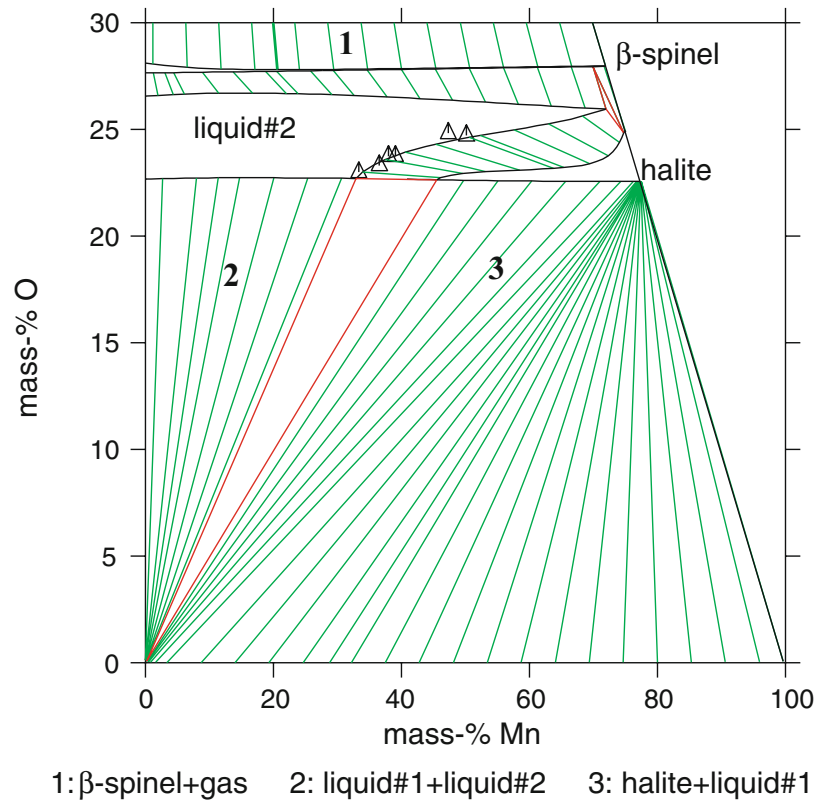


Fig. 17 Calculated isothermal section of the Fe-Mn-O system at 1823 K with experimental data from Nölle^[107]

systems need to be assessed. The models in this work are compatible with the models used in a parallel work on the $\text{Al}_2\text{O}_3\text{-CaO-Fe-O-MgO-SiO}_2$ system.^[122,123]

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